

# Chapter 6

## CONTINUOUS-TIME, IMPULSE-MODULATED, AND DISCRETE-TIME SIGNALS

### 6.6 Sampling Theorem

### 6.7 Aliasing

### 6.8 Interrelations

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# Introduction

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# Introduction

- ▶ In order to process a continuous-time signal using digital signal processing methodologies, it is first necessary to convert the continuous-time signal into a discrete-time signal by applying sampling.
- ▶ Sampling obviously entails discarding part of the continuous-time signal and the question will immediately arise as to whether the sampling process will corrupt the signal.
- ▶ It turns out that under a certain condition that is part of the *sampling theorem*, the information content of the continuous-time signal can be fully preserved.

# The Sampling Theorem

- ▶ The sampling theorem states:  
A bandlimited signal  $x(t)$  for which

$$X(j\omega) = 0 \quad \text{for} \quad |\omega| \geq \frac{\omega_s}{2}$$

where  $\omega_s = 2\pi/T$ , can be uniquely determined from its values  $x(nT)$ .

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- ▶ Alternatively, in what amounts to the same thing, a continuous-time signal whose spectrum is zero outside the baseband (i.e.,  $-\omega_s/2$  to  $\omega_s/2$ ) can, in theory, be recovered completely from an impulse-modulated version of the signal.

## The Sampling Theorem *Cont'd*

- ▶ Consider a two-sided bandlimited signal whose spectrum satisfies the condition of the sampling theorem.

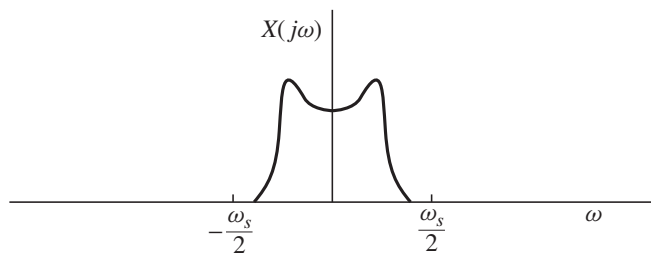
## The Sampling Theorem *Cont'd*

- ▶ Consider a two-sided bandlimited signal whose spectrum satisfies the condition of the sampling theorem.
- ▶ By virtue of Poisson's summation formula, i.e.,

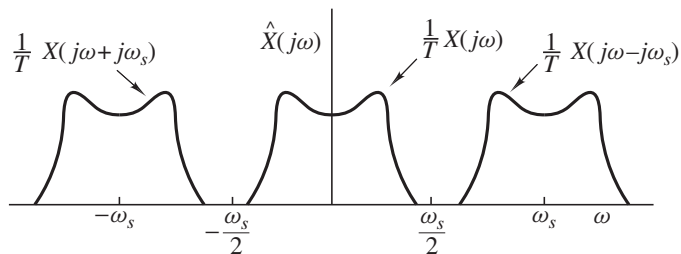
$$\hat{X}(j\omega) = \frac{1}{T} \sum_{n=-\infty}^{\infty} X(j\omega + jn\omega_s)$$

impulse modulation will produce sidebands that are well separated from one another.

# The Sampling Theorem *Cont'd*



(a)



(b)

## The Sampling Theorem *Cont'd*

- ▶ Now if we pass the impulse-modulated signal through an ideal lowpass filter with a frequency response

$$H(j\omega) = \begin{cases} T & \text{for } \omega < \omega_s/2 \\ 0 & \text{otherwise} \end{cases}$$

then frequencies in the sidebands will be rejected and we will be left with the frequencies in the baseband, which constitute the original continuous-time signal.

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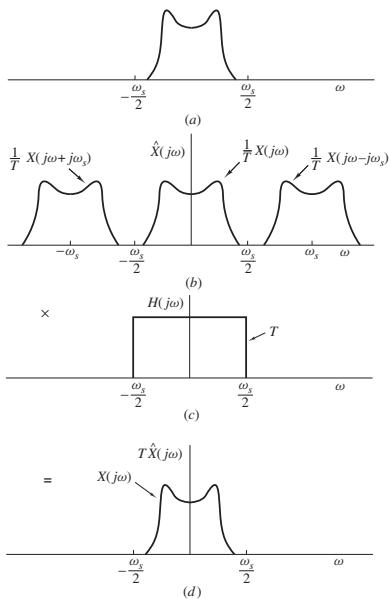
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- ▶ A baseband gain of  $T$  is used to cancel out the scaling constant  $1/T$  introduced by Poisson's summation formula.

# The Sampling Theorem *Cont'd*



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- ▶ What has been done through a graphical illustration can now be repeated with mathematics.

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- ▶ What has been done through a graphical illustration can now be repeated with mathematics.
- ▶ If the impulse-modulated signal is passed through a lowpass filter with a frequency response  $H(j\omega)$  as defined before, then the Fourier transform of the output of the filter will be

$$Y(j\omega) = H(j\omega)\hat{X}(j\omega)$$

where

$$H(j\omega) = \begin{cases} T & \text{for } \omega < \omega_s/2 \\ 0 & \text{otherwise} \end{cases}$$

and

$$\hat{X}(j\omega) = \frac{1}{T} \sum_{n=-\infty}^{\infty} X(j\omega + jn\omega_s)$$

# The Sampling Theorem *Cont'd*

• • •

$$Y(j\omega) = H(j\omega)\hat{X}(j\omega)$$

► If we apply the inverse Fourier transform, we get

$$\begin{aligned} y(t) &= \mathcal{F}^{-1} \left[ H(j\omega) \sum_{n=-\infty}^{\infty} x(nT) e^{-j\omega nT} \right] \\ &= \sum_{n=-\infty}^{\infty} x(nT) \mathcal{F}^{-1} [H(j\omega) e^{-j\omega nT}] \end{aligned} \quad (\text{A})$$

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- ▶ The frequency response of a lowpass filter is actually a frequency-domain pulse of height  $T$  and base  $\omega_s$ , i.e.,  $H(j\omega) = T p_{\omega_s}(\omega)$  and hence from the table of Fourier transforms, we have

$$\frac{T \sin(\omega_s t/2)}{\pi t} \leftrightarrow H(j\omega) \quad (\text{B})$$

# The Sampling Theorem *Cont'd*

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$$\frac{T \sin(\omega_s t/2)}{\pi t} \leftrightarrow H(j\omega) \quad (\text{B})$$

► From the time-shifting theorem of the Fourier transform

$$\frac{T \sin[\omega_s(t - nT)/2]}{\pi(t - nT)} \leftrightarrow H(j\omega)e^{-j\omega nT} \quad (\text{C})$$

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- Therefore, from Eqs. (A) and (C), we conclude that

$$y(t) = \sum_{n=-\infty}^{\infty} x(nT) \frac{\sin[\omega_s(t - nT)/2]}{\omega_s(t - nT)/2}$$

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- For  $t = nT$ , we have  $y(nT) = x(nT)$  for  $n = 0, 1, \dots, kT$ , and for all other values of  $t$  the output of the lowpass filter is an interpolated version of  $x(t)$  according to the sampling theorem.

# Aliasing

- ▶ If the spectrum of the continuous-time signal does *not* satisfy the condition imposed by the sampling theorem, i.e., if

$$X(j\omega) \neq 0 \quad \text{for} \quad |\omega| \geq \frac{\omega_s}{2}$$

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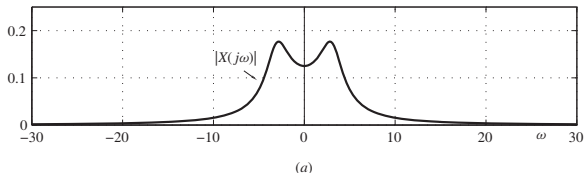
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then sideband frequencies will be aliased into baseband frequencies.

- ▶ As a result,  $\hat{X}(j\omega)$  will not be equal to  $X(j\omega)/T$  within the baseband.
- ▶ Under these circumstances, the use of an ideal lowpass filter will yield a distorted version of  $x(t)$  at best.

- ▶ Aliasing can be illustrated by examining an impulse-modulated signal generated by sampling the continuous-time signal

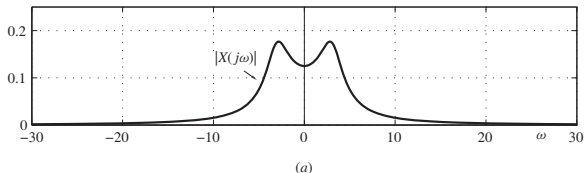
$$x(t) = u(t)e^{-at} \sin \omega_0 t$$



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$$x(t) = u(t)e^{-at} \sin \omega_0 t$$

- ▶ The frequency spectrum of  $x(t)$ ,  $X(j\omega)$ , extends over the infinite range  $-\infty < \omega < \infty$ .



- ▶ The frequency spectrum of impulse-modulated signal  $\hat{x}(t)$  can be obtained as

$$\hat{X}(j\omega) = \frac{1}{T} \sum_{n=-\infty}^{\infty} X(j\omega + jn\omega_s)$$

by using Poisson's summation formula.

• • •

$$\hat{X}(j\omega) = \frac{1}{T} \sum_{n=-\infty}^{\infty} X(j\omega + jn\omega_s)$$

- ▶ The shifted copies of  $X(j\omega)$  or sidebands, namely,  $\dots$ ,  $X(j\omega - j2\omega_s)$ ,  $X(j\omega - j\omega_s)$ ,  $X(j\omega + j\omega_s)$ ,  $X(j\omega + j2\omega_s)$ ,  $\dots$  overlap with the baseband  $-\omega_s/2 < \omega < \omega_s/2$  and, therefore, the above sum can be expressed as

$$\hat{X}(j\omega) = \frac{1}{T} [X(j\omega) + E(j\omega)]$$

where

$$E(j\omega) = \sum_{\substack{k=-\infty \\ k \neq 0}}^{\infty} X(j\omega + jk\omega_s)$$

is the contribution of the sidebands to the baseband.

- ▶ Now if we filter the impulse-modulated signal,  $\hat{x}(t)$ , using an ideal lowpass filter with a frequency response

$$H(j\omega) = \begin{cases} T & \text{for } -\omega_s/2 < \omega < \omega_s/2 \\ 0 & \text{otherwise} \end{cases}$$

we will get a signal  $y(t)$  whose frequency spectrum is given by

$$\begin{aligned} Y(j\omega) &= H(j\omega)\hat{X}(j\omega) \\ &= H(j\omega) \cdot \frac{1}{T} \sum_{n=-\infty}^{\infty} X(j\omega + jn\omega_s) \\ &= X(j\omega) + E(j\omega) \end{aligned}$$

• • •

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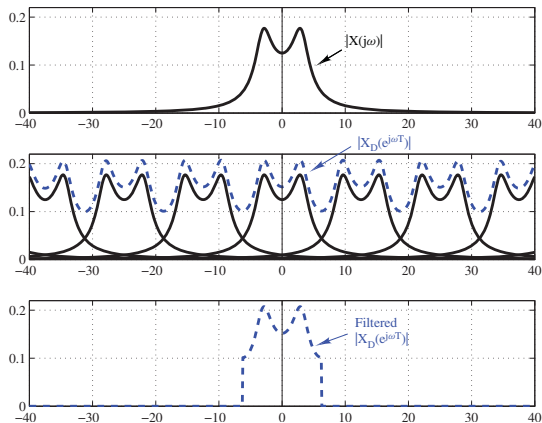
- ▶ In other words, the output of the filter will be signal  $x(t)$  plus an error

$$e(t) = \mathcal{F}^{-1}E(j\omega)$$

which is commonly referred to as the *aliasing error*.

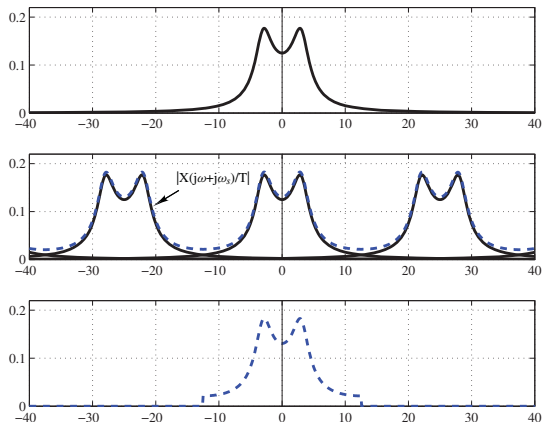
## Aliasing *Cont'd*

- ▶ With a sampling frequency of 12.5 rad/s,  $|E(j\omega)|$ , i.e., the discrepancy between the solid and dashed curves in the figure is quite large.



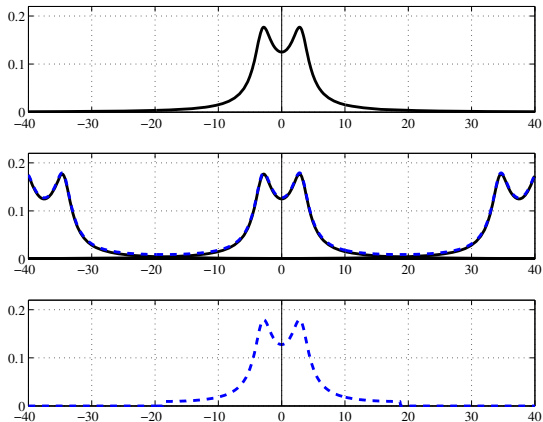
## Aliasing *Cont'd*

- ▶ As the sampling frequency is increased to 25, the sidebands are spread out and  $|E(j\omega)|$  will be decreased quite a bit as shown.



## Aliasing *Cont'd*

- ▶ A further increase to 40 rad/s will render  $|E(j\omega)|$  for all practical purposes negligible as can be seen.



# Summary of Interrelations

- ▶ Impulse-modulate signal:

$$\hat{x}(t) = \sum_{n=-\infty}^{\infty} x(nT)\delta(t - nT) \quad (6.42c)$$

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- ▶ Impulse-modulate signal:

$$\hat{x}(t) = \sum_{n=-\infty}^{\infty} x(nT)\delta(t - nT) \quad (6.42c)$$

- ▶ Spectrum of impulse modulated signal or discrete-time signal in terms of the spectrum of the original continuous-time signal:

$$\hat{X}(j\omega) = X_D(e^{j\omega T}) = \frac{1}{T} \sum_{n=-\infty}^{\infty} X(j\omega + jn\omega_s) \quad (6.45a)$$

where

$$X_D(e^{j\omega T}) = \sum_{n=-\infty}^{\infty} x(nT)e^{-j\omega nT}$$

## Summary of Interrelations *Cont'd*

- ▶ Spectrum of impulse-modulated signal (or discrete-time signal) in terms of the spectrum of the original continuous-time signal for a *right-sided signal*:

$$\hat{X}(j\omega) = X_D(e^{j\omega T}) = \frac{x(0+)}{2} + \frac{1}{T} \sum_{n=-\infty}^{\infty} X(j\omega + jn\omega_s) \quad (6.45b)$$

## Summary of Interrelations *Cont'd*

- ▶ Spectrum of impulse-modulated signal (or discrete-time signal) in terms of the spectrum of the original continuous-time signal for a *right-sided signal*:

$$\hat{X}(j\omega) = X_D(e^{j\omega T}) = \frac{x(0+)}{2} + \frac{1}{T} \sum_{n=-\infty}^{\infty} X(j\omega + jn\omega_s) \quad (6.45b)$$

- ▶ Laplace transform of impulse-modulated signal in terms of the Laplace transform of the original continuous-time signal for a *right-sided signal*:

$$\hat{X}(s) = X_D(z) = \frac{x(0+)}{2} + \frac{1}{T} \sum_{n=-\infty}^{\infty} X(s + jn\omega_s) \quad (6.46a)$$

where  $z = e^{sT}$ .

## Summary of Interrelations *Cont'd*

- ▶ Recovery of a continuous-time signal by lowpass filtering an impulse-modulated filter – *frequency domain*:

$$Y(j\omega) = H(j\omega)\hat{X}(j\omega) \quad (6.48)$$

where

$$H(j\omega) = \begin{cases} T & \text{for } |\omega| < \omega_s/2 \\ 0 & \text{for } |\omega| \geq \omega_s/2 \end{cases}$$

## Summary of Interrelations *Cont'd*

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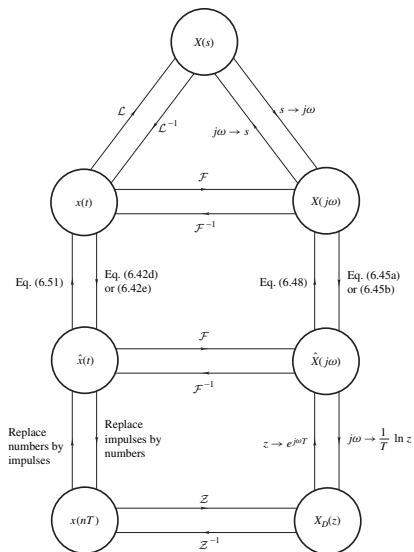
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- ▶ Recovery of a continuous-time signal by lowpass filtering an impulse-modulated filter – *time-domain*:

$$y(t) = \sum_{n=-\infty}^{\infty} x(nT) \frac{\sin[\omega_s(t - nT)/2]}{\omega_s(t - nT)/2} \quad (6.51)$$

# Graphical Representation of Interrelations



*This slide concludes the presentation.  
Thank you for your attention.*