

# JOINTLY OPTIMIZED ERROR-FEEDBACK AND REALIZATION FOR ROUNDOFF NOISE MINIMIZATION IN STATE-ESTIMATE FEEDBACK DIGITAL CONTROLLERS

*Takao Hinamoto, Keijiro Kawai  
and Masayoshi Nakamoto*

Graduate School of Engineering, Hiroshima University  
Higashi-Hiroshima 739-8527, Japan  
phone:+81-82-424-7672, fax:+81-82-422-7195  
email:{hinamoto, msy}@hiroshima-u.ac.jp

*Wu-Sheng Lu*

Dept. of Elect. & Comput. Engineering,  
University of Victoria  
Victoria, B.C., V8W 3P6, Canada  
phone:+1-250-721-8692, fax:+1-250-721-6052  
email: wslu@ece.uvic.ca

## ABSTRACT

The joint optimization problem of error-feedback and realization for the closed-loop system with a state-estimate feedback digital controller is investigated where the main objective is to minimize the effects of roundoff noise at the closed-loop system output subject to  $l_2$ -norm dynamic-range scaling constraints. It is shown that the problem can be converted into an unconstrained optimization problem by using linear-algebraic techniques. The unconstrained optimization problem at hand is then solved iteratively by employing an efficient quasi-Newton algorithm with closed-form formulas for key gradient evaluation. Analytical details are given as to how the proposed technique can be applied to the cases where the error-feedback matrix is a general, diagonal, or scalar matrix. A numerical example is presented to illustrate the utility of the proposed technique.

## 1. INTRODUCTION

Due to the finite precision nature of computer arithmetic, the output roundoff noise of a fixed-point IIR digital filter usually arises. This noise is critically dependent on the internal structure of an IIR digital filter [1],[2]. Error feedback (EF) is known as an effective technique for reducing the output roundoff noise in an IIR digital filter [3]-[5]. Williamson [6] has reduced the output roundoff noise more effectively by choosing the filter structure and applying EF to the filter. Lu and Hinamoto [7] have developed a jointly optimized technique of EF and realization to minimize the effects of roundoff noise at the filter output subject to  $l_2$ -scaling constraints. Li and Gevers [8] have analyzed the output roundoff noise of the closed-loop system with a state-estimate feedback controller, and presented an algorithm for realizing the state-estimate feedback controller with minimum output roundoff noise under  $l_2$ -norm dynamic-range scaling constraints. Hinamoto and Yamamoto [9] have proposed a method for applying EF to a given closed-loop system with a state-estimate feedback controller.

This paper investigates the problem of jointly optimizing EF and realization for the closed-loop system with a state-estimate feedback controller so as to

minimize the output roundoff noise subject to  $l_2$ -norm dynamic-range scaling constraints. To this end, an iterative technique which relies on an efficient quasi-Newton algorithm [10] is developed. Our computer simulation results demonstrate the validity and effectiveness of the proposed technique.

## 2. ROUNDOFF NOISE ANALYSIS

Let a stable, controllable and observable linear discrete-time system be described by

$$\begin{aligned} \mathbf{x}(k+1) &= \mathbf{A}_o \mathbf{x}(k) + \mathbf{b}_o u(k) \\ y(k) &= \mathbf{c}_o \mathbf{x}(k) \end{aligned} \quad (1)$$

where  $\mathbf{x}(k)$  is an  $n \times 1$  state-variable vector,  $u(k)$  is a scalar input,  $y(k)$  is a scalar output, and  $\mathbf{A}_o$ ,  $\mathbf{b}_o$  and  $\mathbf{c}_o$  are real constant matrices of appropriate dimensions. The transfer function of the linear system in (1) is given by

$$H_o(z) = \mathbf{c}_o(z\mathbf{I}_n - \mathbf{A}_o)^{-1}\mathbf{b}_o. \quad (2)$$

If a regulator is designed by using the full-order state observer, we obtain a state-estimate feedback controller as

$$\begin{aligned} \tilde{\mathbf{x}}(k+1) &= \mathbf{F}_o \tilde{\mathbf{x}}(k) + \mathbf{b}_o u(k) + \mathbf{g}_o y(k) \\ &= \mathbf{R}_o \tilde{\mathbf{x}}(k) + \mathbf{b}_o r(k) + \mathbf{g}_o y(k) \\ u(k) &= -\mathbf{k}_o \tilde{\mathbf{x}}(k) + r(k) \end{aligned} \quad (3)$$

where  $\tilde{\mathbf{x}}(k)$  is an  $n \times 1$  state-variable vector in the full-order state observer,  $\mathbf{g}_o$  is an  $n \times 1$  gain vector chosen so that all the eigenvalues of  $\mathbf{F}_o = \mathbf{A}_o - \mathbf{g}_o \mathbf{c}_o$  are inside the unit circle in the complex plane,  $\mathbf{k}_o$  is a  $1 \times n$  state-feedback gain vector chosen so that each of the eigenvalues of  $\mathbf{A}_o - \mathbf{b}_o \mathbf{k}_o$  is at a desirable location within the unit circle,  $r(k)$  is a scalar reference signal, and  $\mathbf{R}_o = \mathbf{F}_o - \mathbf{b}_o \mathbf{k}_o$ .

Performing quantization before matrix-vector multiplication, we can express the finite-word-length (FWL) implementation of (3) with error feedback as

$$\begin{aligned} \hat{\mathbf{x}}(k+1) &= \mathbf{R} \mathbf{Q}[\hat{\mathbf{x}}(k)] + \mathbf{b} r(k) + \mathbf{g} y(k) + \mathbf{D} e(k) \\ u(k) &= -\mathbf{k} \mathbf{Q}[\hat{\mathbf{x}}(k)] + r(k) \end{aligned} \quad (4)$$

where  $e(k) = \hat{\mathbf{x}}(k) - \mathbf{Q}[\hat{\mathbf{x}}(k)]$  and  $\mathbf{D}$  is an  $n \times n$  error feedback matrix. All coefficient matrices  $\mathbf{R}$ ,  $\mathbf{b}$  and  $\mathbf{k}$

are assumed to have an exact fractional  $B_c$  bit representation. The FWL state-variable vector  $\hat{\mathbf{x}}(k)$  and signal  $u(k)$  all have a  $B$  bit fractional representation, while the reference input  $r(k)$  is a  $(B - B_c)$  bit fraction. The vector quantizer  $Q[\cdot]$  in (4) rounds the  $B$  bit fraction  $\tilde{\mathbf{x}}(k)$  to  $(B - B_c)$  bits after completing the multiplications and additions, where the sign bit is not counted. It is assumed that the roundoff error  $\mathbf{e}(k)$  can be modeled as a zero-mean noise process with covariance  $\sigma^2 \mathbf{I}_n$ .

The closed-loop control system consisting of the linear system in (1) and the state-estimate feedback controller in (4) is illustrated in Fig. 1. This closed-loop

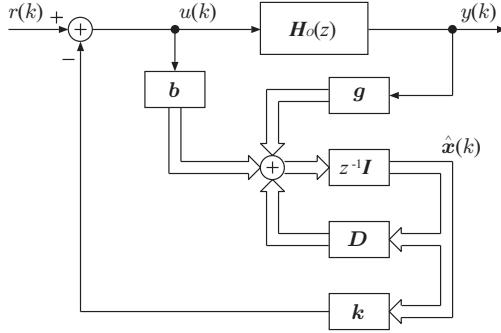


Fig. 1. The closed-loop control system with a state-estimate feedback controller.

system is described by

$$\begin{aligned} \begin{bmatrix} \mathbf{x}(k+1) \\ \hat{\mathbf{x}}(k+1) \end{bmatrix} &= \bar{\mathbf{A}} \begin{bmatrix} \mathbf{x}(k) \\ \hat{\mathbf{x}}(k) \end{bmatrix} + \bar{\mathbf{b}} r(k) + \bar{\mathbf{B}} \mathbf{e}(k) \\ y(k) &= \bar{\mathbf{c}} \begin{bmatrix} \mathbf{x}(k) \\ \hat{\mathbf{x}}(k) \end{bmatrix} \end{aligned} \quad (5)$$

where

$$\begin{aligned} \bar{\mathbf{A}} &= \begin{bmatrix} \mathbf{A}_o & -\mathbf{b}_o \mathbf{k} \\ \mathbf{g} \mathbf{c}_o & \mathbf{R} \end{bmatrix}, & \bar{\mathbf{b}} &= \begin{bmatrix} \mathbf{b}_o \\ \mathbf{b} \end{bmatrix} \\ \bar{\mathbf{B}} &= \begin{bmatrix} \mathbf{b}_o \mathbf{k} \\ \mathbf{D} - \mathbf{R} \end{bmatrix}, & \bar{\mathbf{c}} &= [\mathbf{c}_o \quad \mathbf{0}] \end{aligned}$$

Let the transfer function from the roundoff noise  $\mathbf{e}(k)$  to the output  $y(k)$  in (5) be defined by  $\mathbf{G}_D(z)$ . Then

$$\mathbf{G}_D(z) = \bar{\mathbf{c}} (z \mathbf{I}_{2n} - \bar{\mathbf{A}})^{-1} \bar{\mathbf{B}}. \quad (6)$$

The noise gain  $J(\mathbf{D}) = \sigma_{out}^2 / \sigma^2$  is then computed as

$$J(\mathbf{D}) = \text{tr}[\mathbf{W}_D] \quad (7)$$

with

$$\mathbf{W}_D = \frac{1}{2\pi j} \oint_{|z|=1} \mathbf{G}_D^*(z) \mathbf{G}_D(z) \frac{dz}{z} \quad (8)$$

where  $\sigma_{out}^2$  stands for the noise variance of the output. For tractability, we evaluate  $J(\mathbf{D})$  in (7) by replacing  $\mathbf{R}$ ,  $\mathbf{b}$ ,  $\mathbf{g}$  and  $\mathbf{k}$  by  $\mathbf{R}_o$ ,  $\mathbf{b}_o$ ,  $\mathbf{g}_o$  and  $\mathbf{k}_o$ , respectively. Define

$$\mathbf{S} = \begin{bmatrix} \mathbf{I}_n & \mathbf{0} \\ \mathbf{I}_n & -\mathbf{I}_n \end{bmatrix}, \quad (9)$$

the transfer function  $\mathbf{G}_D(z)$  in (6) can be expressed as

$$\begin{aligned} \mathbf{G}_D(z) &= \bar{\mathbf{c}} \mathbf{S} (z \mathbf{I}_{2n} - \mathbf{S}^{-1} \bar{\mathbf{A}} \mathbf{S})^{-1} \mathbf{S}^{-1} \bar{\mathbf{B}} \\ &= \bar{\mathbf{c}} (z \mathbf{I}_{2n} - \Phi)^{-1} \begin{bmatrix} \mathbf{b}_o \mathbf{k}_o \\ \mathbf{F}_o - \mathbf{D} \end{bmatrix} \\ &= \mathbf{c}_o (z \mathbf{I}_n - \mathbf{A}_o + \mathbf{b}_o \mathbf{k}_o)^{-1} \mathbf{b}_o \mathbf{k}_o (z \mathbf{I}_n - \mathbf{F}_o)^{-1} \\ &\quad \cdot (z \mathbf{I}_n - \mathbf{D}) \\ &= \bar{\mathbf{c}} (z \mathbf{I}_{2n} - \Phi)^{-1} \mathbf{U} (z \mathbf{I}_n - \mathbf{D}) \end{aligned} \quad (10)$$

where

$$\Phi = \begin{bmatrix} \mathbf{A}_o - \mathbf{b}_o \mathbf{k}_o & \mathbf{b}_o \mathbf{k}_o \\ \mathbf{0} & \mathbf{F}_o \end{bmatrix}, \quad \mathbf{U} = \begin{bmatrix} \mathbf{0} \\ \mathbf{I}_n \end{bmatrix}.$$

It is noted that the stability of the closed-loop control system is determined by the eigenvalues of matrix  $\bar{\mathbf{A}}$  in (5), or equivalently, those of matrix  $\Phi$  in (10). This means that neither of the quantization error  $\mathbf{e}(k)$  and the error-feedback matrix  $\mathbf{D}$  affects the stability.

Substituting (10) into matrix  $\mathbf{W}_D$  in (8) gives

$$\begin{aligned} \mathbf{W}_D &= (\mathbf{b}_o \mathbf{k}_o)^T \mathbf{W}_1 \mathbf{b}_o \mathbf{k}_o + (\mathbf{b}_o \mathbf{k}_o)^T \mathbf{W}_2 (\mathbf{F}_o - \mathbf{D}) \\ &\quad + (\mathbf{F}_o - \mathbf{D})^T \mathbf{W}_3 \mathbf{b}_o \mathbf{k}_o \\ &\quad + (\mathbf{F}_o - \mathbf{D})^T \mathbf{W}_4 (\mathbf{F}_o - \mathbf{D}) \end{aligned} \quad (11)$$

where

$$\mathbf{W} = \Phi^T \mathbf{W} \Phi + \bar{\mathbf{c}}^T \bar{\mathbf{c}}, \quad \mathbf{W} = \begin{bmatrix} \mathbf{W}_1 & \mathbf{W}_2 \\ \mathbf{W}_3 & \mathbf{W}_4 \end{bmatrix}.$$

Since  $\mathbf{W}$  is positive semidefinite, it can be shown that there exists an  $n \times n$  matrix  $\mathbf{P}$  such that  $\mathbf{W}_3 = \mathbf{W}_4 \mathbf{P}$ . In addition, (11) can be written by virtue of  $\mathbf{W}_2 = \mathbf{W}_3^T$  as

$$\begin{aligned} \mathbf{W}_D &= (\mathbf{F}_o + \mathbf{P} \mathbf{b}_o \mathbf{k}_o - \mathbf{D})^T \mathbf{W}_4 (\mathbf{F}_o + \mathbf{P} \mathbf{b}_o \mathbf{k}_o - \mathbf{D}) \\ &\quad + (\mathbf{b}_o \mathbf{k}_o)^T (\mathbf{W}_1 - \mathbf{P}^T \mathbf{W}_4 \mathbf{P}) \mathbf{b}_o \mathbf{k}_o. \end{aligned} \quad (12)$$

Alternatively, applying  $z$ -transform to the first equation in (5) under the assumption that  $\mathbf{e}(k) = \mathbf{0}$ , we obtain

$$\begin{bmatrix} \mathbf{X}(z) \\ \hat{\mathbf{X}}(z) \end{bmatrix} = (z \mathbf{I} - \bar{\mathbf{A}})^{-1} \bar{\mathbf{b}} R(z) \quad (13)$$

where  $\mathbf{X}(z)$ ,  $\hat{\mathbf{X}}(z)$  and  $R(z)$  represent the  $z$ -transforms of  $\mathbf{x}(k)$ ,  $\hat{\mathbf{x}}(k)$  and  $r(k)$ , respectively. Replacing  $\mathbf{R}$ ,  $\mathbf{b}$ ,  $\mathbf{k}$  and  $\mathbf{g}$  by  $\mathbf{R}_o$ ,  $\mathbf{b}_o$ ,  $\mathbf{k}_o$  and  $\mathbf{g}_o$ , respectively, and then using

$$\mathbf{S}^{-1} \begin{bmatrix} \mathbf{X}(z) \\ \hat{\mathbf{X}}(z) \end{bmatrix} = (z \mathbf{I}_{2n} - \mathbf{S}^{-1} \bar{\mathbf{A}} \mathbf{S})^{-1} \mathbf{S}^{-1} \bar{\mathbf{b}}$$

yield

$$\hat{\mathbf{X}}(z) = \mathbf{X}(z) = \mathbf{F}(z) R(z) \quad (14)$$

where

$$\mathbf{F}(z) = [z \mathbf{I}_n - (\mathbf{A}_o - \mathbf{b}_o \mathbf{k}_o)]^{-1} \mathbf{b}_o.$$

The controllability Gramian  $\mathbf{K}$  defined by

$$\mathbf{K} = \frac{1}{2\pi j} \oint_{|z|=1} \mathbf{F}(z) \mathbf{F}^*(z) \frac{dz}{z} \quad (15)$$

can be obtained by solving the Lyapunov equation

$$\mathbf{K} = (\mathbf{A}_o - \mathbf{b}_o \mathbf{k}_o) \mathbf{K} (\mathbf{A}_o - \mathbf{b}_o \mathbf{k}_o)^T + \mathbf{b}_o \mathbf{b}_o^T. \quad (16)$$

### 3. ROUNDOFF NOISE MINIMIZATION

Consider the system in (4) with  $\mathbf{D} = \mathbf{0}$  and denote it by  $(\mathbf{R}, \mathbf{b}, \mathbf{g}, \mathbf{k})_n$ . By applying a coordinate transformation  $\tilde{\mathbf{x}}'(k) = \mathbf{T}^{-1} \hat{\mathbf{x}}(k)$  to the above system  $(\mathbf{R}, \mathbf{b}, \mathbf{g}, \mathbf{k})_n$ , we obtain a new realization characterized by  $(\tilde{\mathbf{R}}, \tilde{\mathbf{b}}, \tilde{\mathbf{g}}, \tilde{\mathbf{k}})_n$  where

$$\begin{aligned} \tilde{\mathbf{R}} &= \mathbf{T}^{-1} \mathbf{R} \mathbf{T}, & \tilde{\mathbf{b}} &= \mathbf{T}^{-1} \mathbf{b} \\ \tilde{\mathbf{g}} &= \mathbf{T}^{-1} \mathbf{g}, & \tilde{\mathbf{k}} &= \mathbf{k} \mathbf{T}. \end{aligned} \quad (17)$$

For the system in (17), the counterparts of  $\mathbf{W}_i$  for  $i = 1, 2, 3, 4$  are given by

$$\tilde{\mathbf{W}}_i = \mathbf{T}^T \mathbf{W}_i \mathbf{T} \quad (18)$$

and the corresponding noise gain is given by

$$J(\mathbf{D}, \mathbf{T}) = \text{tr}[\tilde{\mathbf{W}}_D] \quad (19)$$

where  $\tilde{\mathbf{W}}_D$  can be obtained using (11) as

$$\begin{aligned} \tilde{\mathbf{W}}_D &= [\mathbf{T}^{-1}(\mathbf{F}_0 + \mathbf{P} \mathbf{b}_0 \mathbf{k}_0) \mathbf{T} - \mathbf{D}]^T \\ &\quad \cdot \mathbf{T}^T \mathbf{W}_4 \mathbf{T} [\mathbf{T}^{-1}(\mathbf{F}_0 + \mathbf{P} \mathbf{b}_0 \mathbf{k}_0) \mathbf{T} - \mathbf{D}] \\ &\quad + \mathbf{T}^T (\mathbf{b}_0 \mathbf{k}_0)^T (\mathbf{W}_1 - \mathbf{P}^T \mathbf{W}_4 \mathbf{P}) \mathbf{b}_0 \mathbf{k}_0 \mathbf{T}. \end{aligned}$$

In addition, (15) can be written as

$$\tilde{\mathbf{K}} = \mathbf{T}^{-1} \mathbf{K} \mathbf{T}^{-T}. \quad (20)$$

As a result, the output roundoff noise minimization problem amounts to obtaining matrices  $\mathbf{D}$  and  $\mathbf{T}$  which jointly minimize  $J(\mathbf{D}, \mathbf{T})$  in (19) subject to the  $l_2$ -scaling constraints specified by

$$(\tilde{\mathbf{K}})_{ii} = (\mathbf{T}^{-1} \mathbf{K} \mathbf{T}^{-T})_{ii} = 1, \quad i = 1, 2, \dots, n. \quad (21)$$

To deal with (21), we define

$$\hat{\mathbf{T}} = \mathbf{T}^T \mathbf{K}^{-\frac{1}{2}}. \quad (22)$$

Then the  $l_2$ -scaling constraints in (21) can be written as

$$(\hat{\mathbf{T}}^{-T} \hat{\mathbf{T}}^{-1})_{ii} = 1, \quad i = 1, 2, \dots, n. \quad (23)$$

These constraints are always satisfied if  $\hat{\mathbf{T}}^{-1}$  assumes the form

$$\hat{\mathbf{T}}^{-1} = \left[ \frac{\mathbf{t}_1}{\|\mathbf{t}_1\|}, \frac{\mathbf{t}_2}{\|\mathbf{t}_2\|}, \dots, \frac{\mathbf{t}_n}{\|\mathbf{t}_n\|} \right]. \quad (24)$$

Substituting (22) into (19), we obtain

$$\begin{aligned} J(\mathbf{D}, \hat{\mathbf{T}}) &= \text{tr} \left[ \hat{\mathbf{T}} (\hat{\mathbf{A}} - \hat{\mathbf{T}}^T \mathbf{D} \hat{\mathbf{T}}^{-T})^T \hat{\mathbf{W}}_4 \right. \\ &\quad \left. \cdot (\hat{\mathbf{A}} - \hat{\mathbf{T}}^T \mathbf{D} \hat{\mathbf{T}}^{-T}) \hat{\mathbf{T}}^T + \hat{\mathbf{T}} \hat{\mathbf{C}} \hat{\mathbf{T}}^T \right] \end{aligned} \quad (25)$$

where

$$\begin{aligned} \hat{\mathbf{A}} &= \mathbf{K}^{-\frac{1}{2}} (\mathbf{F}_0 + \mathbf{P} \mathbf{b}_0 \mathbf{k}_0) \mathbf{K}^{\frac{1}{2}}, & \hat{\mathbf{W}}_4 &= \mathbf{K}^{\frac{1}{2}} \mathbf{W}_4 \mathbf{K}^{\frac{1}{2}} \\ \hat{\mathbf{C}} &= \mathbf{K}^{\frac{1}{2}} (\mathbf{b}_0 \mathbf{k}_0)^T (\mathbf{W}_1 - \mathbf{P}^T \mathbf{W}_4 \mathbf{P}) \mathbf{b}_0 \mathbf{k}_0 \mathbf{K}^{\frac{1}{2}}. \end{aligned}$$

From the foregoing arguments, the problem of obtaining matrices  $\mathbf{D}$  and  $\mathbf{T}$  that minimize (19) subject to the scaling constraints in (21) is now converted into an unconstrained optimization problem of obtaining  $\mathbf{D}$  and  $\hat{\mathbf{T}}$  that jointly minimize  $J(\mathbf{D}, \hat{\mathbf{T}})$  in (25).

Let  $\mathbf{x}$  be the column vector that collects the variables in matrices  $\mathbf{D}$  and  $[\mathbf{t}_1, \mathbf{t}_2, \dots, \mathbf{t}_n]$ . Then  $J(\mathbf{D}, \hat{\mathbf{T}})$  is a function of  $\mathbf{x}$ , denoted by  $J(\mathbf{x})$ . The proposed algorithm starts with an initial point  $\mathbf{x}_0$  obtained from an initial assignment  $\mathbf{D} = \hat{\mathbf{T}} = \mathbf{I}_n$ . In the  $k$ th iteration, a quasi-Newton algorithm updates the most recent point  $\mathbf{x}_k$  to point  $\mathbf{x}_{k+1}$  as [10]

$$\mathbf{x}_{k+1} = \mathbf{x}_k + \alpha_k \mathbf{d}_k, \quad (26)$$

where

$$\mathbf{d}_k = -\mathbf{S}_k \nabla J(\mathbf{x}_k)$$

$$\alpha_k = \arg \left[ \min_{\alpha} J(\mathbf{x}_k + \alpha \mathbf{d}_k) \right]$$

$$\mathbf{S}_{k+1} = \mathbf{S}_k + \left( 1 + \frac{\boldsymbol{\gamma}_k^T \mathbf{S}_k \boldsymbol{\gamma}_k}{\boldsymbol{\delta}_k^T \boldsymbol{\delta}_k} \right) \frac{\boldsymbol{\delta}_k \boldsymbol{\delta}_k^T}{\boldsymbol{\gamma}_k^T \boldsymbol{\delta}_k} - \frac{\boldsymbol{\delta}_k \boldsymbol{\gamma}_k^T \mathbf{S}_k + \mathbf{S}_k \boldsymbol{\gamma}_k \boldsymbol{\delta}_k^T}{\boldsymbol{\gamma}_k^T \boldsymbol{\delta}_k}$$

$$\mathbf{S}_0 = \mathbf{I}, \quad \boldsymbol{\delta}_k = \mathbf{x}_{k+1} - \mathbf{x}_k, \quad \boldsymbol{\gamma}_k = \nabla J(\mathbf{x}_{k+1}) - \nabla J(\mathbf{x}_k).$$

Here,  $\nabla J(\mathbf{x})$  is the gradient of  $J(\mathbf{x})$  with respect to  $\mathbf{x}$ , and  $\mathbf{S}_k$  is a positive-definite approximation of the inverse Hessian matrix of  $J(\mathbf{x}_k)$ . This iteration process continues until

$$|J(\mathbf{x}_{k+1}) - J(\mathbf{x}_k)| < \varepsilon \quad (27)$$

where  $\varepsilon > 0$  is a prescribed tolerance.

In what follows, we derive closed-form expressions of  $\nabla J(\mathbf{x})$  for the cases where  $\mathbf{D}$  assumes the form of a general, diagonal, or scalar matrix.

1) *Case 1:  $\mathbf{D}$  Is a General Matrix:* From (25), the optimal choice of  $\mathbf{D}$  is given by

$$\mathbf{D} = \hat{\mathbf{T}}^{-T} \hat{\mathbf{A}} \hat{\mathbf{T}}^T, \quad (28)$$

which leads to

$$J(\hat{\mathbf{T}}^{-T} \hat{\mathbf{A}} \hat{\mathbf{T}}^T, \hat{\mathbf{T}}) = \text{tr} \left[ \hat{\mathbf{T}} \hat{\mathbf{C}} \hat{\mathbf{T}}^T \right]. \quad (29)$$

In this case, the number of elements in vector  $\mathbf{x}$  consisting of  $\hat{\mathbf{T}}$  is equal to  $n^2$  and the gradient of  $J(\mathbf{x})$  is found to be

$$\begin{aligned} \frac{\partial J(\mathbf{x})}{\partial t_{ij}} &= \lim_{\Delta \rightarrow 0} \frac{J(\hat{\mathbf{T}}_{ij}) - J(\hat{\mathbf{T}})}{\Delta} \\ &= 2 \mathbf{e}_j^T \hat{\mathbf{T}} \hat{\mathbf{C}} \hat{\mathbf{T}}^T \hat{\mathbf{T}} \mathbf{g}_{ij}, \quad i, j = 1, 2, \dots, n \end{aligned} \quad (30)$$

where  $\hat{\mathbf{T}}_{ij}$  is the matrix obtained from  $\hat{\mathbf{T}}$  with a perturbed  $(i,j)$ th component, which is given by

$$\hat{\mathbf{T}}_{ij} = \hat{\mathbf{T}} + \frac{\Delta \hat{\mathbf{T}} \mathbf{g}_{ij} \mathbf{e}_j^T \hat{\mathbf{T}}}{1 - \Delta \mathbf{e}_j^T \hat{\mathbf{T}} \mathbf{g}_{ij}}$$

and  $\mathbf{g}_{ij}$  is computed using

$$\mathbf{g}_{ij} = \partial \left\{ \frac{\mathbf{t}_j}{\|\mathbf{t}_j\|} \right\} / \partial t_{ij} = \frac{1}{\|\mathbf{t}_j\|^3} (t_{ij} \mathbf{t}_j - \|\mathbf{t}_j\|^2 \mathbf{e}_i).$$

2) *Case 2:  $\mathbf{D}$  Is a Diagonal Matrix:* Here, matrix  $\mathbf{D}$  assumes the form

$$\mathbf{D} = \text{diag}\{d_1, d_2, \dots, d_n\}. \quad (31)$$

In this case, (25) becomes

$$J(\mathbf{D}, \hat{\mathbf{T}}) = \text{tr} [\hat{\mathbf{T}} \mathbf{M}_d \hat{\mathbf{T}}^T] \quad (32)$$

where

$$\begin{aligned} \mathbf{M}_d &= \hat{\mathbf{C}} + \hat{\mathbf{A}}^T \hat{\mathbf{W}}_4 \hat{\mathbf{A}} + \hat{\mathbf{W}}_4 \hat{\mathbf{T}}^T \mathbf{D}^2 \hat{\mathbf{T}}^{-T} \\ &\quad - \hat{\mathbf{A}}^T \hat{\mathbf{W}}_4 \hat{\mathbf{T}}^T \mathbf{D} \hat{\mathbf{T}}^{-T} - \hat{\mathbf{W}}_4 \hat{\mathbf{A}} \hat{\mathbf{T}}^T \mathbf{D} \hat{\mathbf{T}}^{-T}. \end{aligned}$$

It follows that

$$\begin{aligned} \frac{\partial J(\mathbf{x})}{\partial t_{ij}} &= 2\mathbf{e}_j^T \hat{\mathbf{T}} \mathbf{M}_d \hat{\mathbf{T}}^T \hat{\mathbf{T}} \mathbf{g}_{ij}, \quad i, j = 1, 2, \dots, n \\ \frac{\partial J(\mathbf{x})}{\partial d_i} &= 2\mathbf{e}_i^T (\mathbf{D} \hat{\mathbf{T}} - \hat{\mathbf{T}} \hat{\mathbf{A}}^T) \hat{\mathbf{W}}_4 \hat{\mathbf{T}}^T \mathbf{e}_i, \quad i = 1, 2, \dots, n. \end{aligned} \quad (33)$$

3) *Case 3:  $\mathbf{D}$  Is a Scalar Matrix:* It is assumed here that  $\mathbf{D} = \alpha \mathbf{I}_n$  with a scalar  $\alpha$ . The gradient of  $J(\mathbf{x})$  can then be calculated as

$$\begin{aligned} \frac{\partial J(\mathbf{x})}{\partial t_{ij}} &= 2\mathbf{e}_j^T \hat{\mathbf{T}} \mathbf{M}_s \hat{\mathbf{T}}^T \hat{\mathbf{T}} \mathbf{g}_{ij}, \quad i, j = 1, 2, \dots, n \\ \frac{\partial J(\mathbf{x})}{\partial \alpha} &= \text{tr} [\hat{\mathbf{T}} (2\alpha \hat{\mathbf{W}}_4 - \hat{\mathbf{A}}^T \hat{\mathbf{W}}_4 - \hat{\mathbf{W}}_4 \hat{\mathbf{A}}) \hat{\mathbf{T}}^T] \end{aligned} \quad (34)$$

where

$$\mathbf{M}_s = (\hat{\mathbf{A}} - \alpha \mathbf{I}_n)^T \hat{\mathbf{W}}_4 (\hat{\mathbf{A}} - \alpha \mathbf{I}_n) + \hat{\mathbf{C}}.$$

#### 4. A NUMERICAL EXAMPLE

In this section we illustrate the proposed method by considering a linear discrete-time system specified by

$$\begin{aligned} \mathbf{A}_o &= \begin{bmatrix} 0 & 1 & 0 \\ 0 & 0 & 1 \\ 0.339377 & -1.152652 & 1.520167 \end{bmatrix}, \quad \mathbf{b}_o = \begin{bmatrix} 0 \\ 0 \\ 1 \end{bmatrix} \\ \mathbf{c}_o &= [0.093253 \ 0.128620 \ 0.314713]. \end{aligned}$$

Suppose that the poles of the observer and regulator in the system are required to be located at  $z = 0.1532, 0.2861, 0.1137$ , and  $z = 0.5067, 0.6023, 0.4331$ , respectively. This can be achieved by choosing

$$\begin{aligned} \mathbf{k}_o &= [0.471552 \ -0.367158 \ 3.062267] \\ \mathbf{g}_o &= [-0.006436 \ 3.683651 \ 5.083920]^T. \end{aligned}$$

Performing the  $l_2$ -scaling to the state-estimate feedback controller, we obtain  $J(\mathbf{0}) = 686.4121$  in (7) where  $\mathbf{D} = \mathbf{0}$ . Next, the controller is transformed into the optimal realization that minimizes  $J(\mathbf{0})$  in (7) under the  $l_2$ -scaling constraints. This leads to  $J_{min}(\mathbf{0}) = 28.6187$ . Finally, EF and state-variable coordinate transformation are applied to the above optimal realization so as to jointly minimize the output roundoff noise. The profiles of  $J(\mathbf{x})$  during the first 20 iteration for the cases of  $\mathbf{D}$  being a general, diagonal, and scalar matrix are depicted in Fig. 2.

1) *Case 1:  $\mathbf{D}$  Is a General Matrix:* The quasi-Newton algorithm was applied to minimize (25). It took the algorithm 20 iterations to converge to the solution

$$\begin{aligned} \mathbf{D} &= \begin{bmatrix} 0.211191 & -3.078211 & -3.344596 \\ -1.321589 & 1.897308 & 3.243515 \\ 1.917916 & -1.890027 & -3.807473 \end{bmatrix} \\ \mathbf{T} &= \begin{bmatrix} -11.039974 & -43.683697 & -30.131793 \\ -3.231505 & 8.919473 & 9.118205 \\ 2.620911 & 6.462685 & 7.032260 \end{bmatrix} \end{aligned}$$

and the minimized noise gain was found to be  $J(\mathbf{D}, \hat{\mathbf{T}}) = 4.8823$ . Next, the above optimal EF matrix  $\mathbf{D}$  was rounded to a power-of-two representation with 3 bits after the binary point, which resulted in

$$\mathbf{D}_{3bit} = \begin{bmatrix} 0.250 & -3.125 & -3.375 \\ -1.375 & 1.875 & 3.250 \\ 1.875 & -1.875 & -3.750 \end{bmatrix}$$

and a noise gain  $J(\mathbf{D}_{3bit}, \hat{\mathbf{T}}) = 23.4873$ . Furthermore, when the optimal EF matrix  $\mathbf{D}$  was rounded to the integer representation

$$\mathbf{D}_{int} = \begin{bmatrix} 0 & -3 & -3 \\ -1 & 2 & 3 \\ 2 & -2 & -4 \end{bmatrix},$$

the noise gain was found to be  $J(\mathbf{D}_{int}, \hat{\mathbf{T}}) = 293.0187$ .

2) *Case 2:  $\mathbf{D}$  Is a Diagonal Matrix:* Again, the quasi-Newton algorithm was applied to minimize  $J(\mathbf{D}, \hat{\mathbf{T}})$  in (25) for a diagonal EF matrix  $\mathbf{D}$ . It took the algorithm 20 iterations to converge to the solution

$$\begin{aligned} \mathbf{D} &= \text{diag}\{0.050638, -0.608845, -0.951572\} \\ \mathbf{T} &= \begin{bmatrix} 3.588878 & 0.735966 & 0.010417 \\ -2.457241 & 0.728171 & 0.556762 \\ 1.514232 & -2.058856 & 0.142204 \end{bmatrix} \end{aligned}$$

and the minimized noise gain was found to be  $J(\mathbf{D}, \hat{\mathbf{T}}) = 12.7097$ . Next, the above optimal diagonal EF matrix  $\mathbf{D}$  was rounded to a power-of-two representation with 3 bits after the binary point to yield  $\mathbf{D}_{3bit} = \text{diag}\{0.000, -0.625, -1.000\}$ , which leads to a noise gain  $J(\mathbf{D}_{3bit}, \hat{\mathbf{T}}) = 12.7722$ . Furthermore, when the optimized diagonal EF matrix  $\mathbf{D}$  was rounded to the integer representation  $\mathbf{D}_{int} = \text{diag}\{0, -1, -1\}$ , the noise gain was found to be  $J(\mathbf{D}_{int}, \hat{\mathbf{T}}) = 13.7535$ .

3) *Case 3:  $\mathbf{D}$  Is a Scalar Matrix:* In this case, the quasi-Newton algorithm was applied to minimize (25)

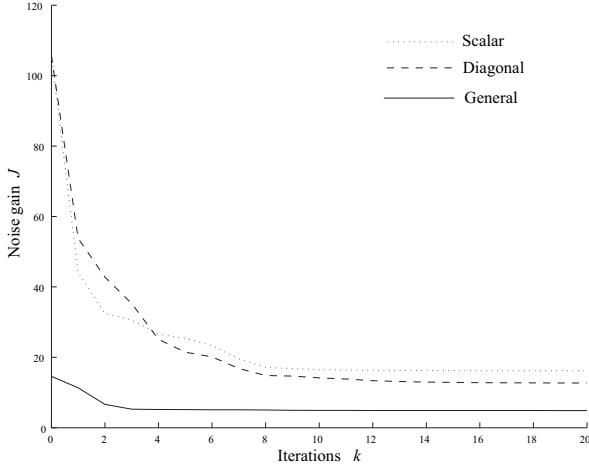


Fig. 2. Profiles of iterative noise gain minimization.

for  $\mathbf{D} = \alpha\mathbf{I}_3$  with a scalar  $\alpha$ . The algorithm converges after 20 iterations to converge to the solution

$$\mathbf{D} = -0.779678\mathbf{I}_3$$

$$\mathbf{T} = \begin{bmatrix} 3.252790 & -0.081745 & -0.198376 \\ -1.717225 & 1.220068 & -0.792487 \\ 0.546599 & -0.854316 & 2.295944 \end{bmatrix}$$

and the minimized noise gain was found to be  $J(\mathbf{D}, \hat{\mathbf{T}}) = 16.2006$ . Next, the EF matrix  $\mathbf{D} = \alpha\mathbf{I}_3$  was rounded to a power-of-two representation with 3 bits after the binary point as well as an integer representation. It was found that these representations were given by  $\mathbf{D}_{3bit} = \text{diag}\{0.750, 0.750, 0.750\}$  and  $\mathbf{D}_{int} = \text{diag}\{1, 1, 1\}$ , respectively. The corresponding noise gains were obtained as  $J(\mathbf{D}_{3bit}, \hat{\mathbf{T}}) = 16.2370$  and  $J(\mathbf{D}_{int}, \hat{\mathbf{T}}) = 18.2063$ , respectively.

The above simulation results in terms of noise gain  $J(\mathbf{D}, \hat{\mathbf{T}})$  in (25) are summarized in Table 1. For comparison purpose, their counterparts obtained using the method in [9] are also included in the table, where the minimization of the roundoff noise was carried out using EF and state-variable coordinate transformation, but in a separate manner. From the table, it is observed that the proposed joint optimization offers improved reduction in roundoff noise gain for the cases of a scalar EF matrix and a diagonal EF matrix when compared with those obtained by using *separate* optimization. However, in the case of a general EF matrix, the optimal solution with infinite precision appears to be quite sensitive to the parameter perturbations.

More reduction of the noise gain might be possible by re-designing the coordinate transformation matrix  $\mathbf{T}$  for the optimally quantized  $\mathbf{D}$ .

## 5. CONCLUSION

The joint optimization problem of EF and realization to minimize the effects of roundoff noise of the closed-loop system with a state-estimate feedback controller subject to  $l_2$ -scaling constraints has been investigated. The problem at hand has been converted into an unconstrained optimization problem by using linear alge-

Table 1: Noise gain  $J(\mathbf{D}, \hat{\mathbf{T}})$  for different EF schemes.

Error-Feedback Scheme	Accuracy of $\mathbf{D}$		
	Infinite Precision	3 Bit Quantization	Integer Quantization
$\mathbf{D} = \mathbf{0}$ Separate	28.6187		
Scalar Separate [9]	20.1235	20.1810	26.0527
Scalar Joint	16.2006	16.2370	18.2063
Diagonal Separate [9]	16.4104	16.4547	17.4039
Diagonal Joint	12.7097	12.7722	13.7535
General Separate [9]	11.6352	11.7054	16.5814
General Joint	4.8823	23.4873	293.0187

braic techniques. An efficient quasi-Newton algorithm has been employed to solve the unconstrained optimization problem. The proposed technique has been applied to the cases where EF matrix is a general, diagonal, or scalar matrix. The effectiveness for the cases of a scalar EF matrix and a diagonal EF matrix compared with the existing method [9] has been illustrated by a numerical example.

## REFERENCES

- [1] C. T. Mullis and R. A. Roberts, "Synthesis of minimum roundoff noise fixed point digital filters," *IEEE Trans. Circuits Syst.*, vol. CAS-23, pp. 551-562, Sept. 1976.
- [2] S. Y. Hwang, "Minimum uncorrelated unit noise in state-space digital filtering," *IEEE Trans. Acoust. Speech, Signal Processing*, vol. ASSP-25, pp. 273-281, Aug. 1977.
- [3] W. E. Higgins and D. C. Munson, "Optimal and suboptimal error-spectrum shaping for cascade-form digital filters," *IEEE Trans. Circuits Syst.*, vol. CAS-31, pp. 429-437, May 1984.
- [4] T. I. Laakso and I. O. Hartimo, "Noise reduction in recursive digital filters using high-order error feedback," *IEEE Trans. Signal Processing*, vol. 40, pp. 1096-1107, May 1992.
- [5] P. P. Vaidyanathan, "On error-spectrum shaping in state-space digital filters," *IEEE Trans. Circuits Syst.*, vol. CAS-32, pp. 88-92, Jan. 1985.
- [6] D. Williamson, "Roundoff noise minimization and pole-zero sensitivity in fixed-point digital filters using residue feedback," *IEEE Trans. Acoust. Speech, Signal Processing*, vol. ASSP-34, pp. 1210-1220, Oct. 1986.
- [7] W.-S. Lu and T. Hinamoto, "Jointly optimized error-feedback and realization for roundoff noise minimization in state-space digital filters," *IEEE Trans. Signal Processing*, vol. 53, pp. 2135-2145, June 2005.
- [8] G. Li and M. Gevers, "Optimal finite precision implementation of a state-estimate feedback controller," *IEEE Trans. Circuits Syst.*, vol. CAS-37, pp. 1487-1498, Dec. 1990.
- [9] T. Hinamoto and S. Yamamoto, "Error spectrum shaping in closed-loop systems with state-estimate feedback controller," in *Proc. IEEE Int. Symp. Circuits Syst. (ISCAS'02)*, May 2002, vol. 1, pp. 289-292.
- [10] R. Fletcher, *Practical Methods of Optimization*, 2nd ed. New York: Wiley, 1987.