

Chapter 9

REALIZATION

9.2.3 State-Space Realization

9.2.4 Lattice Realization

9.2.5 Cascade Realization

9.2.6 Parallel Realization

9.2.7 Transposition

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July 10, 2018

State-Space Realization

- Another approach to the realization of digital filters is to start with the state-space characterization:

$$\begin{aligned}\mathbf{q}(nT + T) &= \mathbf{A}\mathbf{q}(nT) + \mathbf{b}x(nT) \\ y(nT) &= \mathbf{c}^T \mathbf{q}(nT) + dx(nT)\end{aligned}$$

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- The state-space equations can be written as

$$\begin{aligned}q_i(nT + T) &= \sum_{j=1}^N a_{ij}q_j(nT) + b_i x(nT) \quad \text{for } i = 1, 2, \dots, N \\ y(nT) &= \sum_{j=1}^N c_j q_j(nT) + d_0 x(nT)\end{aligned}$$

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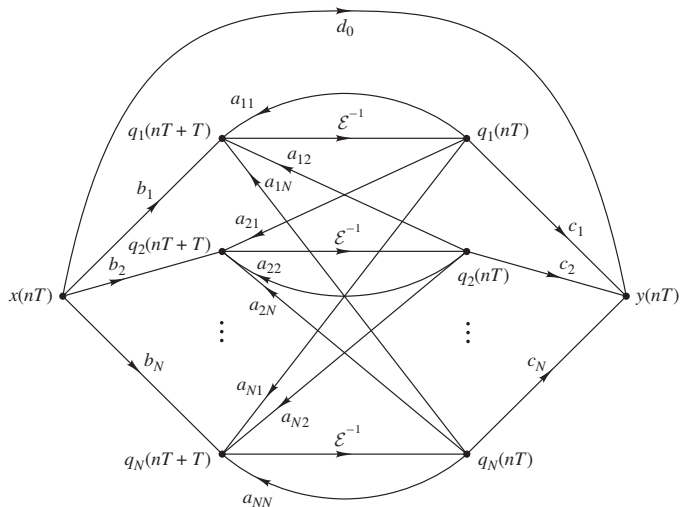
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- A realization can now be obtained by converting the signal flow graph for the state-space equations into a network.

State-Space Realization *Cont'd*



Example

A discrete-time system can be represented by the state-space equations

$$\begin{aligned}\mathbf{q}(nT + T) &= \mathbf{A}\mathbf{q}(nT) + \mathbf{b}x(nT) \\ y(nT) &= \mathbf{c}^T \mathbf{q}(nT) + dx(nT)\end{aligned}$$

where

$$\mathbf{A} = \begin{bmatrix} m_1 & 0 \\ 0 & m_2 \end{bmatrix}, \mathbf{b} = \begin{bmatrix} 1 \\ 1 \end{bmatrix}, \mathbf{c} = \begin{bmatrix} m_1 \\ m_2 \end{bmatrix}, d = 2$$

Obtain a state-space realization.

Example *Cont'd*

Solution For a general second-order system, we have

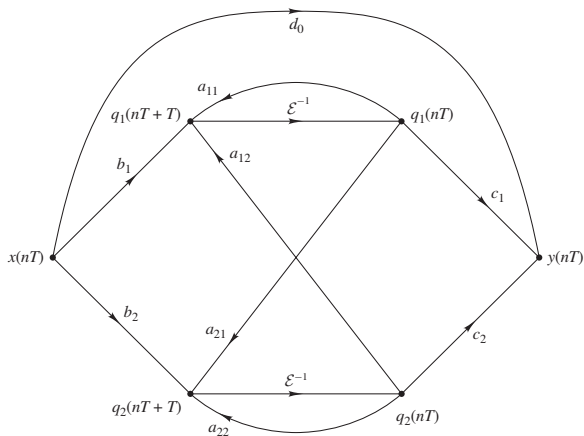
$$\mathbf{A} = \begin{bmatrix} a_{11} & a_{12} \\ a_{21} & a_{22} \end{bmatrix}, \quad \mathbf{b} = \begin{bmatrix} b_1 \\ b_2 \end{bmatrix}, \quad \mathbf{c} = \begin{bmatrix} c_1 \\ c_2 \end{bmatrix}, \quad d = d_0$$

Hence the state-space equations can be expressed as

$$\begin{aligned} q_1(nT + T) &= a_{11}q_1(nT) + a_{12}q_2(nT) + b_1x(nT) \\ q_2(nT + T) &= a_{21}q_1(nT) + a_{22}q_2(nT) + b_2x(nT) \\ y(nT) &= c_1q_1(nT) + c_2(nT)q_2(nT) + dx(nT) \end{aligned}$$

Example *Cont'd*

Signal flow graph:



Example *Cont'd*

For the problem at hand, we have

$$a_{11} = m_1, \quad a_{12} = 0, \quad a_{21} = 0, \quad a_{22} = m_2$$

$$b_1 = 1, \quad b_2 = 1, \quad c_1 = m_1, \quad c_2 = m_2, \quad d_0 = 2$$

The required network can be obtained by replacing summing nodes by adders, distribution nodes by distribution nodes, and transmittances by multipliers and unit delays as appropriate. ■

State-Space Realization *Cont'd*

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- However, they also offer certain advantages, as follows:

State-Space Realization *Cont'd*

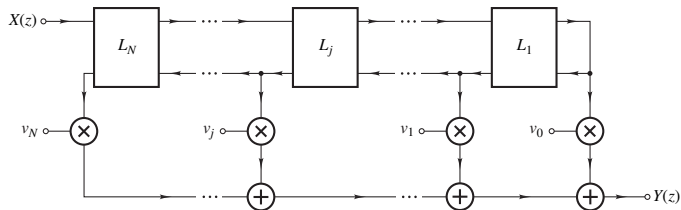
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 - Reduced signal-to-noise ratios can be achieved.

State-Space Realization *Cont'd*

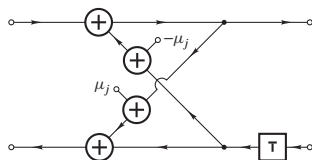
- State-space structures tend to require more elements.
- However, they also offer certain advantages, as follows:
 - Reduced signal-to-noise ratios can be achieved.
 - A certain type of oscillations due to nonlinearities, known as *parasitic oscillations* can be eliminated in these structures (see Chap. 14).

Lattice Realization

- The lattice method was proposed by Gray and Markel and it is based on the configuration shown.



(a)



(b)

- A transfer function of the form

$$H(z) = \frac{N(z)}{D(z)} = \frac{\sum_{i=0}^N a_i z^{-i}}{1 + \sum_{i=1}^N b_i z^{-i}}$$

can be realized by applying a step-by-step recursive algorithm comprising N iterations to obtain a series of polynomials of the form

$$N_j(z) = \sum_{i=0}^j \alpha_{ji} z^{-i} \quad \text{and} \quad D_j(z) = \sum_{i=0}^j \beta_{ji} z^{-i}$$

for $j = N, N - 1, \dots, 0$.

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for $j = N, N - 1, \dots, 0$.

- Then for each value of j the multiplier constants ν_j and μ_j are evaluated using coefficients α_{jj} and β_{jj} in the above polynomials.

1. Let $N_j(z) = N(z)$ and $D_j(z) = D(z)$ and assume that $j = N$, that is

$$N_N(z) = \sum_{i=0}^j \alpha_{ji} z^{-i} = \sum_{i=0}^N a_i z^{-i}$$

$$D_N(z) = \sum_{i=0}^j \beta_{ji} z^{-i} = \sum_{i=0}^N b_i z^{-i} \quad \text{with } b_0 = 1$$

...

$$N_N(z) = \sum_{i=0}^j \alpha_{ji} z^{-i} = \sum_{i=0}^N a_i z^{-i} \quad \text{and} \quad D_N(z) = \sum_{i=0}^j \beta_{ji} z^{-i} = \sum_{i=0}^N b_i z^{-i}$$

2. Obtain ν_j , μ_j , $N_{j-1}(z)$, and $D_{j-1}(z)$ for $j = N, N-1, \dots, 2$ using the following recursive relations:

$$\nu_j = \alpha_{jj}, \quad \mu_j = \beta_{jj}$$

$$P_j(z) = D_j \left(\frac{1}{z} \right) z^{-j} = \sum_{i=0}^j \beta_{ji} z^{i-j}$$

$$N_{j-1}(z) = N_j(z) - \nu_j P_j(z) = \sum_{i=0}^{j-1} \alpha_{ji} z^{-i}$$

$$D_{j-1}(z) = \frac{D_j(z) - \mu_j P_j(z)}{1 - \mu_j^2} = \sum_{i=0}^{j-1} \beta_{ji} z^{-i}$$

3. Obtain ν_1 , μ_1 , and $N_0(z)$ as follows:

$$\nu_1 = \alpha_{11}, \quad \mu_1 = \beta_{11}$$

$$P_1(z) = D_1 \left(\frac{1}{z} \right) z^{-1} = \beta_{10}z^{-1} + \beta_{11}$$

$$N_0(z) = N_1(z) - \nu_1 P_1(z) = \alpha_{00}$$

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4. Complete the realization by letting

$$\nu_0 = \alpha_{00}$$

Example

Realize the transfer function

$$H(z) = \frac{a_0 + a_1z^{-1} + a_2z^{-2}}{1 + b_1z^{-1} + b_2z^{-2}}$$

using the lattice method.

Solution

Step 1 We can write

$$N_2(z) = \alpha_{20} + \alpha_{21}z^{-1} + \alpha_{22}z^{-2} = a_0 + a_1z^{-1} + a_2z^{-2}$$

$$D_2(z) = \beta_{20} + \beta_{21}z^{-1} + \beta_{22}z^{-2} = 1 + b_1z^{-1} + b_2z^{-2}$$

Example *Cont'd*

Step 2: For $j = 2$, we get

$$\nu_2 = \alpha_{22} = a_2 \quad \mu_2 = \beta_{22} = b_2$$

$$P_2(z) = D_2 \left(\frac{1}{z} \right) z^{-2} = z^{-2} + b_1 z^{-1} + b_2 = \beta_{20} z^{-2} + \beta_{21} z^{-1} + \beta_{22}$$

$$\begin{aligned} N_1(z) &= N_2(z) - \nu_2 P_2(z) = a_0 + a_1 z^{-1} + a_2 z^{-2} - \nu_2 (z^{-2} + b_1 z^{-1} + b_2) \\ &= \alpha_{10} + \alpha_{11} z^{-1} \end{aligned}$$

$$\begin{aligned} D_1(z) &= \frac{D_2(z) - \mu_2 P_2(z)}{1 - \mu_2^2} = \frac{1 + b_1 z^{-1} + b_2 z^{-2} - \mu_2 (z^{-2} + b_1 z^{-1} + b_2)}{1 - \mu_2^2} \\ &= \beta_{10} + \beta_{11} z^{-1} \end{aligned}$$

where

$$\begin{aligned} \alpha_{10} &= a_0 - a_2 b_2 & \alpha_{11} &= a_1 - a_2 b_1 \\ \beta_{10} &= 1, & \beta_{11} &= \frac{b_1}{1 + b_2} \end{aligned}$$

Example *Cont'd*

Step 3 Similarly, for $j = 1$ we have

$$\nu_1 = \alpha_{11} = a_1 - a_2 b_1 \quad \mu_1 = \beta_{11} = \frac{b_1}{1 + b_2}$$

$$P_1(z) = D_1 \left(\frac{1}{z} \right) z^{-1} = \beta_{10} z^{-1} + \beta_{11}$$

$$N_0(z) = N_1(z) - \nu_1 P_1(z) = \alpha_{10} + \alpha_{11} z^{-1} - \nu_1 (\beta_{10} z^{-1} + \beta_{11}) = \alpha_{00}$$

where

$$\alpha_{00} = (a_0 - a_2 b_2) - \frac{(a_1 - a_2 b_1) b_1}{1 + b_2}$$

Example *Cont'd*

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where

$$\alpha_{00} = (a_0 - a_2 b_2) - \frac{(a_1 - a_2 b_1) b_1}{1 + b_2}$$

Step 4: Finally, step 4 gives

$$\nu_0 = \alpha_{00}$$

Example *Cont'd*

Summarizing, the multiplier constants for a general second-order lattice realization are as follows:

$$\begin{aligned}\nu_0 &= (a_0 - a_2 b_2) - \frac{(a_1 - a_2 b_1)b_1}{1 + b_2} \\ \nu_1 &= a_1 - a_2 b_1, \quad \nu_2 = a_2 \\ \mu_1 &= \frac{b_1}{1 + b_2}, \quad \mu_2 = b_2\end{aligned}$$

Lattice Realization *Cont'd*

- A problem associated with the lattice configuration presented is that it requires a large number of multipliers.

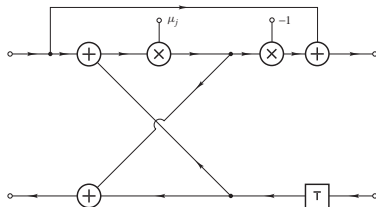
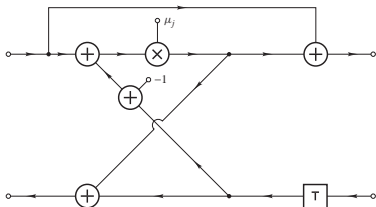
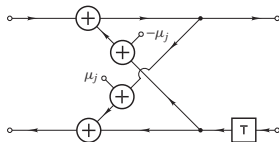
Lattice Realization *Cont'd*

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Lattice Realization *Cont'd*

- A problem associated with the lattice configuration presented is that it requires a large number of multipliers.
- Fortunately, a more economical lattice structure is possible.
- It turns out that the 2-multiplier lattice module shown earlier can be replaced by one of two 1-multiplier lattice modules as shown in the next slide.

Lattice Realization *Cont'd*



Lattice Realization *Cont'd*

- Parameters μ_j for $j = 1, 2, \dots, N$ stay the same as before.

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- However, parameters ν_j need to be recalculated as

$$\tilde{\nu}_j = \frac{\nu_j}{\xi_j}$$

where

$$\xi_j = \begin{cases} 1 & \text{for } j = N \\ \prod_{i=j}^{N-1} (1 + \varepsilon_i \mu_{i+1}) & \text{for } j = 0, 1, \dots, N-1 \end{cases}$$

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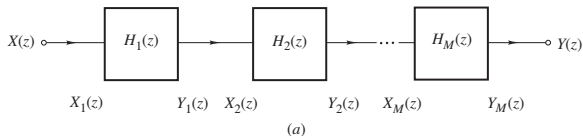
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- Parameter ε_i takes the value of $+1$ or -1 depending on which of the two 1-multiplier lattice modules is used.

Cascade Realization

- Consider an arbitrary number of filter sections connected in cascade as shown and assume that the i th section is characterized by

$$Y_i(z) = H_i(z)X_i(z)$$



Cascade Realization *Cont'd*

- We can write

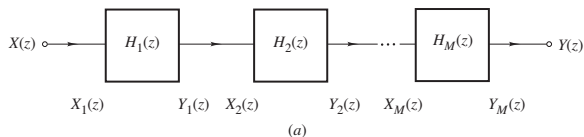
$$Y_1(z) = H_1(z)X_1(z) = H_1(z)X(z)$$

$$Y_2(z) = H_2(z)X_2(z) = H_2(z)Y_1(z) = H_1(z)H_2(z)X(z)$$

$$Y_3(z) = H_3(z)X_3(z) = H_3(z)Y_2(z) = H_1(z)H_2(z)H_3(z)X(z)$$

.....

$$Y(z) = Y_M(z) = H_M(z)Y_{M-1}(z) = H_1(z)H_2(z)\cdots H_M(z)X(z)$$



Cascade Realization *Cont'd*

- Therefore, the overall transfer function of a cascade arrangement of filter sections is equal to the *product* of the individual transfer functions, that is,

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- An N th-order transfer function can be factorized into a product of first- and second-order transfer functions of the form

$$H_i(z) = \frac{a_{0i} + a_{1i}z^{-1}}{1 + b_{1i}z^{-1}} \quad \text{and} \quad H_i(z) = \frac{a_{0i} + a_{1i}z^{-1} + a_{2i}z^{-2}}{1 + b_{1i}z^{-1} + b_{2i}z^{-2}}$$

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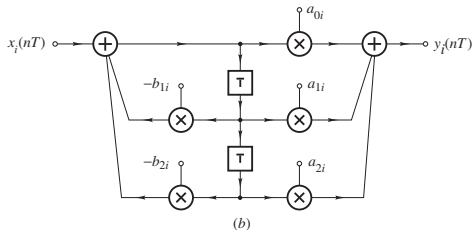
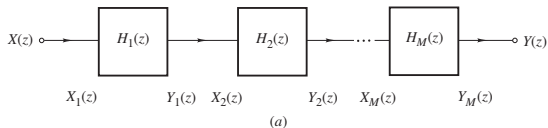
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- Each of these low-order transfer functions can be realized using any one of the methods described.

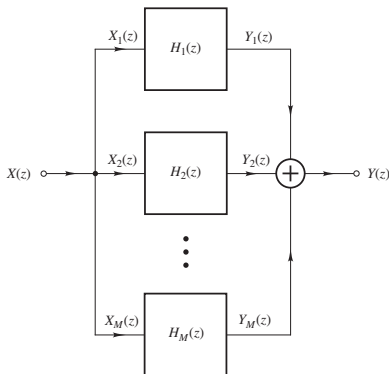
Cascade Realization *Cont'd*

- For example, an arbitrary transfer function can be realized by using a cascade arrangement of canonic sections as shown.



Parallel Realization

- Another realization comprising first- and second-order filter sections is based on the parallel configuration shown.



Parallel Realization *Cont'd*

- We note that all the parallel sections have a common input, i.e., $X_1(z) = X_2(z) = \cdots = X_M(z) = X(z)$.

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- Hence

$$\begin{aligned} Y(z) &= Y_1(z) + Y_2(z) + \dots + Y_M(z) \\ &= H_1(z)X_1(z) + H_2(z)X_2(z) + \dots + H_M(z)X_M(z) \\ &= H_1(z)X(z) + H_2(z)X(z) + \dots + H_M(z)X(z) \\ &= [H_1(z) + H_2(z) + \dots + H_M(z)]X(z) \\ &= H(z)X(z) \end{aligned}$$

where

$$H(z) = \sum_{i=1}^M H_i(z)$$

Example

Obtain a parallel realization of the transfer function

$$H(z) = \frac{10z^4 - 3.7z^3 - 1.28z^2 + 0.99z}{(z^2 - z + 0.34)(z^2 + 0.9z + 0.2)}$$

using canonic sections.

Solution The transfer function can be expressed as

$$H(z) = \frac{10z^4 - 3.7z^3 - 1.28z^2 + 0.99z}{(z - p_1)(z - p_2)(z - p_3)(z - p_4)}$$

where

$$p_1, p_2 = 0.5 \mp j0.3$$

$$p_3 = -0.4$$

$$p_4 = -0.5$$

Example *Cont'd*

If we expand $H(z)/z$ into partial fractions, we get

$$\frac{H(z)}{z} = \frac{R_1}{z - 0.5 + j0.3} + \frac{R_2}{z - 0.5 - j0.3} + \frac{R_3}{z + 0.4} + \frac{R_4}{z + 0.5}$$

where

$$R_1 = 1, \quad R_2 = 1, \quad R_3 = 3, \quad R_4 = 5$$

Example *Cont'd*

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$$\frac{H(z)}{z} = \frac{R_1}{z - 0.5 + j0.3} + \frac{R_2}{z - 0.5 - j0.3} + \frac{R_3}{z + 0.4} + \frac{R_4}{z + 0.5}$$

where

$$R_1 = 1, \quad R_2 = 1, \quad R_3 = 3, \quad R_4 = 5$$

Thus

$$H(z) = \frac{z}{z - 0.5 + j0.3} + \frac{z}{z - 0.5 - j0.3} + \frac{3z}{z + 0.4} + \frac{5z}{z + 0.5}$$

Example *Cont'd*

...

$$H(z) = \frac{z}{z - 0.5 + j0.3} + \frac{z}{z - 0.5 - j0.3} + \frac{3z}{z + 0.4} + \frac{5z}{z + 0.5}$$

Combining the first two and the last two partial fractions into second-order transfer functions, we get

$$H(z) = H_1(z) + H_2(z)$$

where

$$H_1(z) = \frac{2 - z^{-1}}{1 - z^{-1} + 0.34z^{-2}} \quad \text{and} \quad H_2(z) = \frac{8 + 3.5z^{-1}}{1 + 0.9z^{-1} + 0.2z^{-2}}$$

Example *Cont'd*

...

$$H(z) = \frac{z}{z - 0.5 + j0.3} + \frac{z}{z - 0.5 - j0.3} + \frac{3z}{z + 0.4} + \frac{5z}{z + 0.5}$$

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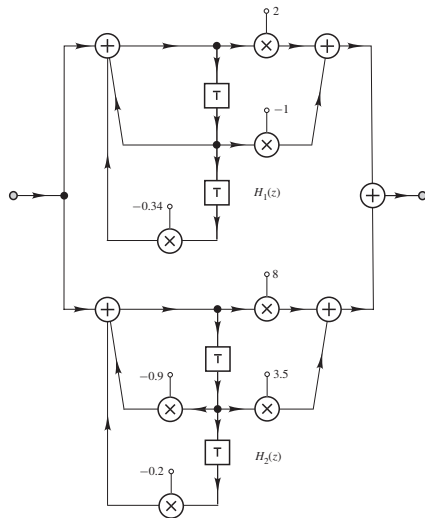
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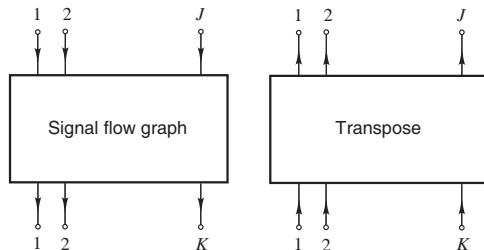
Using canonic structures for the two second-order transfer functions, the structure on the next slide is readily obtained.

Example *Cont'd*



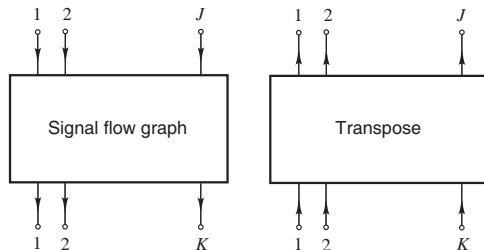
Transpose

- Given a signal flow graph with inputs $j = 1, 2, \dots, J$ and outputs $k = 1, 2, \dots, K$, *a corresponding signal flow graph can be derived* by reversing the direction in each and every branch such that the J input nodes become output nodes and the K output nodes become input nodes.



Transpose

- Given a signal flow graph with inputs $j = 1, 2, \dots, J$ and outputs $k = 1, 2, \dots, K$, a *corresponding signal flow graph can be derived* by reversing the direction in each and every branch such that the J input nodes become output nodes and the K output nodes become input nodes.
- The signal flow graph so derived is said to be the *transpose* of the original signal flow graph.



- If a signal flow graph and its transpose are characterized by transfer functions $H_{jk}(z)$ and $H_{kj}(z)$, respectively, then

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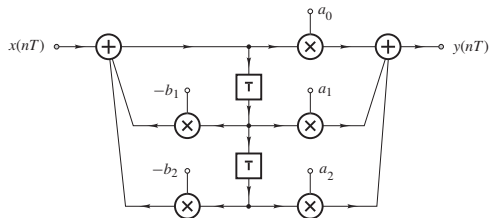
- In effect, given a digital-filter structure a corresponding transpose structure can be obtained that has the *same transfer function*.

- If a signal flow graph and its transpose are characterized by transfer functions $H_{jk}(z)$ and $H_{kj}(z)$, respectively, then

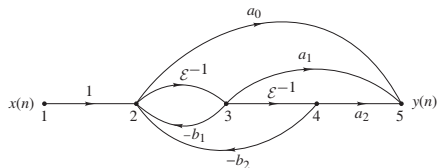
$$H_{jk}(z) = H_{kj}(z)$$

- In effect, given a digital-filter structure a corresponding transpose structure can be obtained that has the *same transfer function*.
- Sometimes, the derived transpose structure has improved features relative to the original structure.

Example

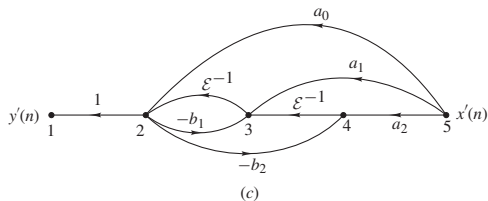
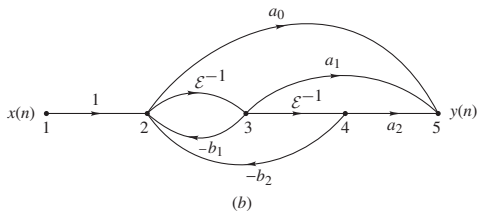


(a)

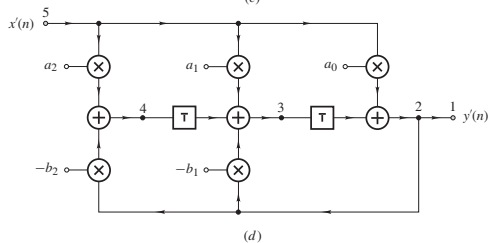
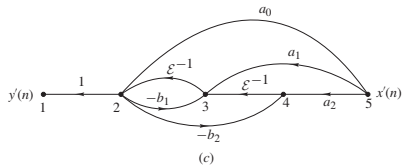


(b)

Example *Cont'd*



Example *Cont'd*



*This slide concludes the presentation.
Thank you for your attention.*