

Roundoff Noise Minimization in Closed-Loop Systems Using Optimal Error Feedback and Realization

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Abstract: We investigate the problem of optimizing error-feedback and realization to minimize the roundoff noise subject to l_2 -scaling constraints in a system in which full-order state observer feedback is used in place of system state feedback. In this paper, the optimal error-feedback matrix is determined in closed-form in advance. As a result, joint optimization of error-feedback and realization is no longer required. An iterative optimization technique for obtaining the optimal coordinate transformation matrix that minimizes the roundoff noise subject to l_2 -scaling constraints is explored by employing a quasi-Newton algorithm. We also describe a separate optimization technique for comparison purposes. The results of numerical experiments demonstrate the validity and effectiveness of the proposed technique.

Keywords: l_2 -scaling, Error feedback, Quasi-Newton method, Realization, Roundoff noise minimization, State observer

1. INTRODUCTION

In fixed-point recursive digital filters, roundoff noise arises due to finite-precision nature of computer arithmetic, and roundoff noise in turn degrades the filters' performance. Error feedback (EF) is well known as an effective method for reducing finite-word-length (FWL) effects in recursive digital filters, and many EF methods have been proposed in the past [1]-[5]. In addition, it is known that the roundoff noise significantly depends on the internal description of the recursive filter, and techniques for realizing a state-space model structure that minimizes the roundoff noise at the filter output subject to l_2 -scaling constraints have been explored by appropriately constructing a linear transformation for state-space coordinates [6],[7]. As a natural extension of the aforementioned methods, efforts have been made to develop new methods that combine EF and realization for achieving better performance [8],[9]. Another relevant development was initiated in [10] where roundoff noise in a closed-loop system equipped with a full-order state observer feedback system is analyzed and an algorithm for realizing a full-order state observer feedback system which minimizes the roundoff noise subject to l_2 -scaling constraints is proposed. It is noted that no EF is incorporated into the algorithm in [10].

This paper investigates the problem of optimizing EF and realization for roundoff noise minimization subject to l_2 -scaling constraints in a system in which full-order state observer feedback is used instead of system state feedback. An iterative optimization technique for obtaining the optimal solution that minimizes the roundoff noise subject to l_2 -scaling constraints is explored by utilizing a quasi-Newton algorithm. Numerical experiments are included to demonstrate the validity and effectiveness of the proposed technique. It is stated that an alternative analytical optimization technique will appear this year [11].

2. NOISE GAIN AS FUNCTION OF ERROR FEEDBACK MATRIX

Suppose that a stable, controllable and observable linear discrete-time system $(F_o, g_o, h_o)_n$ is described by

$$\begin{aligned} x(k+1) &= F_o x(k) + g_o u(k) \\ y(k) &= h_o x(k) \end{aligned} \quad (1)$$

where $x(k)$ is an $n \times 1$ state-variable vector, $u(k)$ is a scalar input, $y(k)$ is a scalar output, and F_o, g_o , and h_o are real constant matrices of $n \times n$, $n \times 1$, and $1 \times n$, respectively. The transfer function of the linear discrete-time system in (1) is expressed as

$$H_o(z) = h_o(zI_n - F_o)^{-1}g_o. \quad (2)$$

Then the full-order state observer and associated state feedback law are modelled as

$$\begin{aligned} \hat{x}(k+1) &= E_o \hat{x}(k) + g_o u(k) + b_o y(k) \\ u(k) &= -f_o \hat{x}(k) + r(k) \end{aligned} \quad (3)$$

where $\hat{x}(k)$ is an $n \times 1$ state-variable vector in the full-order state observer with an $n \times 1$ gain vector b_o , $r(k)$ is a scalar reference signal, f_o is a $1 \times n$ state-feedback coefficient vector and $E_o = F_o - b_o h_o$. It is obvious that the full-order state observer and associated state feedback system in (3) are equivalent to

$$\begin{aligned} \hat{x}(k+1) &= \Phi_o \hat{x}(k) + g_o r(k) + b_o y(k) \\ u(k) &= -f_o \hat{x}(k) + r(k) \end{aligned} \quad (4)$$

where $\Phi_o = F_o - b_o h_o - g_o f_o$.

Next, we consider the FWL implementation of the system due to the quantizations that are carried out before matrix-vector multiplication. At the same time, we assume that an EF is integrated into the system for noise reduction purposes. The model under these circumstances becomes

$$\begin{aligned} \tilde{x}(k+1) &= \Phi Q[\tilde{x}(k)] + g r(k) + b y(k) + C e(k) \\ u(k) &= -f Q[\tilde{x}(k)] + r(k) \end{aligned} \quad (5)$$

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where $e(k) = \tilde{x}(k) - Q[\tilde{x}(k)]$ and C is an $n \times n$ EF matrix. The coefficient matrices Φ , g , b , and f in (5) are representations of Φ_o , g_o , b_o , and f_o , respectively, with exact fractional B_c -bit. The FWL state-variable vector $\tilde{x}(k)$ and each output $u(k)$ in (5) has B -bit fractional representations, while the reference input $r(k)$ and the signal $y(k)$ are $(B - B_c)$ -bit fractions. The quantizer $Q[\cdot]$ in (5) rounds the B -bit fraction $\tilde{x}(k)$ to $(B - B_c)$ -bit after the multiplications and additions, where the sign bit is not counted. It is assumed that the quantization error vector $e(k)$ can be modeled as a Gaussian random process with zero mean and covariance $\sigma^2 I_n$.

The closed-loop system that consists of the systems in (1) and (5) is then described by

$$\begin{aligned} \begin{bmatrix} x(k+1) \\ \tilde{x}(k+1) \end{bmatrix} &= \begin{bmatrix} F_o & -g_o f \\ b h_o & \Phi \end{bmatrix} \begin{bmatrix} x(k) \\ \tilde{x}(k) \end{bmatrix} \\ &+ \begin{bmatrix} g_o \\ g \end{bmatrix} r(k) + \begin{bmatrix} g_o f \\ C - \Phi \end{bmatrix} e(k) \quad (6) \\ y(k) &= \begin{bmatrix} h_o & 0 \end{bmatrix} \begin{bmatrix} x(k) \\ \tilde{x}(k) \end{bmatrix}. \end{aligned}$$

From (6), the transfer function from the quantization error vector $e(k)$ to the output $y(k)$ can be written as

$$H_C(z) = \tilde{h}(zI_{2n} - \tilde{F})^{-1} \tilde{G} \quad (7)$$

where

$$\tilde{F} = \begin{bmatrix} F_o & -g_o f \\ b h_o & \Phi \end{bmatrix}, \quad \tilde{G} = \begin{bmatrix} g_o f \\ C - \Phi \end{bmatrix}, \quad \tilde{h} = \begin{bmatrix} h_o & 0 \end{bmatrix}.$$

Based on the model developed above, we now define the normalized noise gain $J_1(C) = \sigma_{out}^2 / \sigma^2$ in terms of the transfer function $H_C(z)$ in (7) as

$$J_1(C) = \text{tr} \left[\frac{1}{2\pi j} \oint_{|z|=1} H_C^*(z) H_C(z) \frac{dz}{z} \right]. \quad (8)$$

To derive a formula for evaluating the normalized noise gain $J_1(C)$, we replace f , b , and Φ in matrices $\tilde{F}$ and $\tilde{G}$ by their infinite-precision counterparts f_o , b_o , and Φ_o , respectively. Then an approximate version of $H_C(z)$ in (7) is found to be

$$\begin{aligned} H_C(z) &\simeq \tilde{h} S (zI_{2n} - S \tilde{F} S)^{-1} S \tilde{G} \\ &= \tilde{h} (zI_{2n} - \Psi)^{-1} V (zI_n - C) \end{aligned} \quad (9)$$

where

$$S = \begin{bmatrix} I_n & 0 \\ I_n & -I_n \end{bmatrix}, \quad \Psi = \begin{bmatrix} F_o - g_o f_o & g_o f_o \\ 0 & E_o \end{bmatrix}, \quad V = \begin{bmatrix} 0 \\ I_n \end{bmatrix}.$$

Substituting (9) into (8) yields

$$\begin{aligned} J_1(C) &= \text{tr} \left[C^T Y_4 C - (f_o^T g_o^T Y_3^T + E_o^T Y_4) C \right. \\ &\quad \left. - C^T (Y_3 g_o f_o + Y_4 E_o) + Y_4 \right] \quad (10) \end{aligned}$$

where

$$\begin{bmatrix} Y_1 & Y_2 \\ Y_3 & Y_4 \end{bmatrix} = \Psi^T \begin{bmatrix} Y_1 & Y_2 \\ Y_3 & Y_4 \end{bmatrix} \Psi + \begin{bmatrix} h_o^T \\ 0 \end{bmatrix} \begin{bmatrix} h_o & 0 \end{bmatrix}.$$

To reach an adequate formulation for the problem at hand, we derive an explicit expression for the controllability Gramian K for state-variable vector $\tilde{x}(k)$ in system (6), because K is a critical quantity involved in the l_2 -scaling constraints on $\tilde{x}(k)$. To this end, the transfer function from reference input $r(k)$ to state-variable vector $[x(k)^T, \tilde{x}(k)^T]^T$ is derived by setting $e(k) = 0$ in (6) and taking z -transform of (6), i.e.

$$\begin{bmatrix} X(z) \\ \tilde{X}(z) \end{bmatrix} = (zI_{2n} - \tilde{F})^{-1} \begin{bmatrix} g_o \\ g \end{bmatrix} R(z) \quad (11)$$

where $X(z)$ and $\tilde{X}(z)$ denote the z -transforms of $x(k)$ and $\tilde{x}(k)$, respectively. In order to derive a formula for evaluating a good approximate version of the controllability Gramian, we replace matrices Φ , g , f and b in (11) by Φ_o , g_o , f_o and b_o , respectively, which yields

$$S \begin{bmatrix} X(z) \\ \tilde{X}(z) \end{bmatrix} = (zI_{2n} - S \tilde{F} S)^{-1} S \begin{bmatrix} g_o \\ g_o \end{bmatrix} R(z). \quad (12)$$

Hence

$$\tilde{X}(z) = X(z) = F(z) R(z) \quad (13)$$

where $F(z) = [zI_n - (F_o - g_o f_o)]^{-1} g_o$. The controllability Gramian can now be defined as

$$K = \frac{1}{2\pi j} \oint_{|z|=1} F(z) F^*(z) \frac{dz}{z} \quad (14)$$

which can be obtained by solving the Lyapunov equation

$$K = (F_o - g_o f_o) K (F_o - g_o f_o)^T + g_o g_o^T. \quad (15)$$

We are now in a position to consider a family of different yet equivalent state-space descriptions of (4), which can be obtained via coordinate transformation $\bar{x}(k) = T^{-1} \hat{x}(k)$ as $(\bar{\Phi}_o, \bar{g}_o, \bar{b}_o, \bar{f}_o)_n$, where

$$\begin{aligned} \bar{\Phi}_o &= T^{-1} \Phi_o T, & \bar{g}_o &= T^{-1} g_o \\ \bar{b}_o &= T^{-1} b_o, & \bar{f}_o &= f_o T. \end{aligned} \quad (16)$$

Accordingly, the controllability and observability Gramians relating to $(\bar{\Phi}_o, \bar{g}_o, \bar{b}_o, \bar{f}_o)_n$ can be expressed as

$$\bar{K} = T^{-1} K T^{-T}, \quad \bar{Y}_i = T^T Y_i T \quad (17)$$

for $1 \leq i \leq 4$, respectively. In order to prevent the new state-variables from overflow oscillations, the l_2 -scaling constraints are imposed on the state-variable vector $\bar{x}(k)$ so that

$$(\bar{K})_{ii} = (T^{-1} K T^{-T})_{ii} = 1 \text{ for } i = 1, 2, \dots, n. \quad (18)$$

With an equivalent state-space realization as specified in (16), the normalized noise gain is found to be

$$\begin{aligned} J_2(C, T) &= \text{tr} [T^T Y_4 T C C^T] + \text{tr} [T^T Y_4 T] \\ &\quad - 2 \text{tr} [T^T (Y_3 g_o f_o + Y_4 E_o)^T T C]. \end{aligned} \quad (19)$$

The problem considered here is to design the EF matrix C and coordinate transformation matrix T to minimize $J_2(C, T)$ in (19) subject to the l_2 -scaling constraints in (18).

3. OPTIMIZATION OF ERROR FEEDBACK AND REALIZATION

3.1. A Separate Optimization Technique

To perform the first step, define the Lagrange function

$$J(P, \lambda) = \text{tr}[Y_4 P] + \lambda (\text{tr}[K P^{-1}] - n) \quad (20)$$

where $P = T T^T$. The optimal coordinate transformation matrix T can be determined by solving the equations

$$\frac{\partial J(P, \lambda)}{\partial P} = 0, \quad \frac{\partial J(P, \lambda)}{\partial \lambda} = 0 \quad (21)$$

which lead to $P Y_4 P = \lambda K$ and $\text{tr}[K P^{-1}] = n$. Then by some manipulations it follows that

$$P = \frac{1}{n} \left(\sum_{i=1}^n \theta_i \right) Y_4^{-\frac{1}{2}} \left[Y_4^{\frac{1}{2}} K Y_4^{\frac{1}{2}} \right]^{\frac{1}{2}} Y_4^{-\frac{1}{2}} \quad (22)$$

where θ_i^2 denotes the eigenvalue of $K Y_4$. Substituting (22) into (20) yields the minimum value of $J(P, \lambda)$ as

$$\min_{P, \lambda} J(P, \lambda) = \frac{1}{n} \left(\sum_{i=1}^n \theta_i \right)^2. \quad (23)$$

Referring to (22), the optimal coordinate transformation matrix T that minimizes (20) is obtained in a closed form as

$$T = \frac{1}{\sqrt{n}} \left(\sum_{i=1}^n \theta_i \right)^{\frac{1}{2}} Y_4^{-\frac{1}{2}} \left[Y_4^{\frac{1}{2}} K Y_4^{\frac{1}{2}} \right]^{\frac{1}{4}} V_o \quad (24)$$

where V_o is an arbitrary $n \times n$ orthogonal matrix. From (24) we obtain

$$\bar{K} = n \left(\sum_{i=1}^n \theta_i \right)^{-1} V_o^T \left[Y_4^{\frac{1}{2}} K Y_4^{\frac{1}{2}} \right]^{\frac{1}{2}} V_o \quad (25)$$

Next, we choose the $n \times n$ orthogonal matrix V_o such that matrix $\bar{K}$ in (25) satisfies the l_2 -scaling constraints in (18). To this end, we perform the eigenvalue-eigenvector decomposition

$$\left[Y_4^{\frac{1}{2}} K Y_4^{\frac{1}{2}} \right]^{\frac{1}{2}} = Q \text{diag}\{\theta_1, \theta_2, \dots, \theta_n\} Q^T \quad (26)$$

where $Q Q^T = I_n$. As a result, it follows that

$$n \left(\sum_{i=1}^n \theta_i \right)^{-1} \left[Y_4^{\frac{1}{2}} K Y_4^{\frac{1}{2}} \right]^{\frac{1}{2}} = Q \Lambda^{-2} Q^T \quad (27)$$

where

$$\Lambda = \text{diag}\{\lambda_1, \lambda_2, \dots, \lambda_n\}, \quad \lambda_i = \left(\frac{\theta_1 + \theta_2 + \dots + \theta_n}{n \theta_i} \right)^{\frac{1}{2}}.$$

Now, an $n \times n$ orthogonal matrix Z such that

$$(Z \Lambda^{-2} Z^T)_{ii} = 1 \quad \text{for } i = 1, 2, \dots, n \quad (28)$$

can be obtained by numerical manipulations [7, p.278]. By choosing $V_o = Q Z^T$ in (24), the optimal coordinate transformation matrix T satisfying (18) and (23) can be constructed as

$$T = \frac{1}{\sqrt{n}} \left(\sum_{i=1}^n \theta_i \right)^{\frac{1}{2}} Y_4^{-\frac{1}{2}} \left[Y_4^{\frac{1}{2}} K Y_4^{\frac{1}{2}} \right]^{\frac{1}{4}} Q Z^T. \quad (29)$$

Using (19), we compute $\partial J_2(C, T) / \partial C$ and set it to null that leads to

$$C = T^{-1} Y_4^{-1} (Y_3 g_o f_o + Y_4 E_o) T. \quad (30)$$

This provides an analytic method for reducing the round-off noise at the output of a closed-loop system subject to l_2 -scaling constraints by using EF with a general matrix C .

3.2. An Iterative Optimization Technique

The normalized noise gain in (10) is equivalent to

$$J_1(C) = \text{tr} \left[(M - C)^T Y_4 (M - C) + Y_4 - M^T Y_4 M \right] \quad (31)$$

where $M = E_o + L g_o f_o$ and L is an $n \times n$ matrix satisfying $Y_4 L = Y_3$. With an equivalent state-space realization as specified in (16), the normalized noise gain in (31) is changed to

$$J_2(C, T) = \text{tr} \left[(MT - TC)^T Y_4 (MT - TC) + T^T (Y_4 - M^T Y_4 M) T \right]. \quad (32)$$

Because the constraints in (18) are nonconvex and highly nonlinear with respect to matrix T , it is beneficial if these constraints can be eliminated so as to work with an unconstrained problem that admits fast Newton-like algorithms. To this end, we start by defining

$$\hat{T} = T^T K^{-\frac{1}{2}} \quad (33)$$

which leads (18) to

$$(\hat{T}^{-T} \hat{T}^{-1})_{ii} = 1 \quad \text{for } i = 1, 2, \dots, n. \quad (34)$$

These constraints are always satisfied if the matrix $\hat{T}^{-1}$ assumes the form

$$\hat{T}^{-1} = \left[\frac{t_1}{\|t_1\|}, \frac{t_2}{\|t_2\|}, \dots, \frac{t_n}{\|t_n\|} \right]. \quad (35)$$

By virtue of (33), the normalized noise gain in (32) can be expressed as

$$J_3(C, \hat{T}) = \text{tr}[(\hat{M} \hat{T}^T - \hat{T}^T C)^T \hat{Y}_4 (\hat{M} \hat{T}^T - \hat{T}^T C)] + \text{tr}[\hat{T}(\hat{Y}_4 - \hat{M}^T \hat{Y}_4 \hat{M}) \hat{T}^T] \quad (36)$$

where $\hat{M} = K^{-\frac{1}{2}} M K^{\frac{1}{2}}$ and $\hat{Y}_4 = K^{\frac{1}{2}} Y_4 K^{\frac{1}{2}}$. From (36) it is evident that the optimal choice of C is given by

$$C = \hat{T}^{-T} \hat{M} \hat{T}^T \quad (37)$$

which leads to

$$J_3(\hat{T}^{-T} \hat{M} \hat{T}^T, \hat{T}) = \text{tr}[\hat{T}(\hat{Y}_4 - \hat{M}^T \hat{Y}_4 \hat{M}) \hat{T}^T]. \quad (38)$$

The above derivation clearly indicates that the joint optimization of EF and realization is not needed because the optimal C has already been determined by the closed-form in (37), hence it is sufficient to optimize matrix $\hat{T}$ by minimizing $J_3(\hat{T}^{-T} \hat{M} \hat{T}^T, \hat{T})$ in (38).

The solution of minimizing $J_3(\hat{T}^{-T} \hat{M} \hat{T}^T, \hat{T})$ in (38) was found to be fairly sensitive to how the EF matrix C was quantized in the system implementation. As a remedy for this sensitivity issue, we consider a regularized minimization problem with the objective function given by

$$\begin{aligned} J_o(x) &= \mu \text{tr}[\hat{T} \hat{Y}_4 \hat{T}^T] \\ &\quad + (1 - \mu) \text{tr}[\hat{T}(\hat{Y}_4 - \hat{M}^T \hat{Y}_4 \hat{M}) \hat{T}^T] \\ &= \text{tr}[\hat{T}\{\hat{Y}_4 - (1 - \mu) \hat{M}^T \hat{Y}_4 \hat{M}\} \hat{T}^T] \end{aligned} \quad (39)$$

where x is defined by $x = (t_1^T, t_2^T, \dots, t_n^T)^T$ and μ is a regularization parameter in the range $0 < \mu \leq 1$ that can be selected to make an appropriate trade-off between minimizing (38) and reducing $\text{tr}[\hat{T} \hat{Y}_4 \hat{T}^T]$.

The proposed algorithm starts with an initial point x_0 obtained from the assignment $\hat{T} = C = I_n$. In the k th iteration, a quasi-Newton algorithm updates the most recent point x_k to point x_{k+1} as [12]

$$x_{k+1} = x_k + \alpha_k d_k \quad (40)$$

where

$$\begin{aligned} d_k &= -S_k \nabla J_\gamma(x_k), \quad \alpha_k = \arg \min_{\alpha} J_\gamma(x_k + \alpha d_k) \\ S_{k+1} &= S_k + \left(1 + \frac{\varphi_k^T S_k \varphi_k}{\varphi_k^T \delta_k}\right) \frac{\delta_k \delta_k^T}{\varphi_k^T \delta_k} \\ &\quad - \frac{\delta_k \varphi_k^T S_k + S_k \varphi_k \delta_k^T}{\varphi_k^T \delta_k}, \quad S_0 = I \\ \delta_k &= x_{k+1} - x_k, \quad \varphi_k = \nabla J_\gamma(x_{k+1}) - \nabla J_\gamma(x_k). \end{aligned}$$

Here, $\nabla J_o(x)$ is the gradient of $J_o(x)$ with respect to x , and S_k is a positive-definite approximation of the inverse Hessian matrix of $J_o(x_k)$. This iteration process continues until

$$|J_o(x_{k+1}) - J_o(x_k)| < \varepsilon \quad (41)$$

is satisfied where $\varepsilon > 0$ is a prescribed tolerance.

The gradients of $J_o(x)$ with respect to $t_1, t_2, \dots, t_n$ are found to be

$$\frac{\partial J_o(x)}{\partial t_{ij}} = 2e_j^T \hat{T} \{ \hat{Y}_4 - (1 - \mu) \hat{M}^T \hat{Y}_4 \hat{M} \} \hat{T}^T \hat{T} \Delta_{ij}$$

(42)

where t_{ij} is the i th element of column vector t_j , and

$$\Delta_{ij} = -\partial \left\{ \frac{t_j}{\|t_j\|} \right\} / \partial t_{ij} = \frac{1}{\|t_j\|^3} (t_{ij} t_j - \|t_j\|^2 e_i).$$

4. NUMERICAL EXPERIMENTS

Consider a linear discrete-time system specified by

$$\begin{aligned} F_o &= \begin{bmatrix} 0 & 0 & 0.775585 \\ 1 & 0 & -2.534177 \\ 0 & 1 & 2.758200 \end{bmatrix}^T, \quad g_o = \begin{bmatrix} 0 \\ 0 \\ 1 \end{bmatrix} \\ h_o &= [0.0022 \quad 0.0044 \quad 0.0022]. \end{aligned}$$

Suppose that the full-order state observer has the poles at $z = 0.4532, 0.5761$ and 0.8437 , and that the poles of the regulator are placed at $z = 0.9067, 0.7523$ and 0.6231 . Then, the coefficient vector of the full-order state observer and the gain vector of the state feedback were found to be

$$\begin{aligned} b_o &= 100 [0.818859 \quad 1.010891 \quad 1.182995]^T \\ f_o &= [0.350562 \quad -0.818344 \quad 0.476100]. \end{aligned}$$

The controllability and observability Gramians K and Y_4 relating to the closed-loop discrete-time system in (6) were computed from (15) and (10) as

$$\begin{aligned} K &= 10^2 \begin{bmatrix} 4.510584 & 4.474816 & 4.374469 \\ 4.474816 & 4.510584 & 4.474816 \\ 4.374469 & 4.474816 & 4.510584 \end{bmatrix} \\ Y_4 &= 10 \begin{bmatrix} 0.469714 & -1.031460 & 0.556758 \\ -1.031460 & 2.265722 & -1.223243 \\ 0.556758 & -1.223243 & 0.660514 \end{bmatrix}. \end{aligned}$$

By performing l_2 -scaling to the system with

$$T_o = 10 \text{diag}\{2.123814, 2.123814, 2.123814\}$$

so that $(T_o^{-1} K T_o^{-T})_{ii} = 1$ is satisfied for $i = 1, 2, 3$, the normalized noise gain of the system without EF was computed from (10) as

$$J_1(0) = \text{tr}[T_o^T Y_4 T_o] = 1.531772 \times 10^3.$$

The quasi-Newton algorithm was applied to minimize (39) with $\mu = 0.01$ and tolerance $\varepsilon = 10^{-8}$ in (41). The initial normalized noise gain was found to be $J_o(x) = 10.084792 \times 10^{-3}$ and it took the algorithm 15 iterations to converge to the solution

$$\begin{aligned} \hat{T} &= \begin{bmatrix} 1.957936 & 0.179654 & 0.105801 \\ -1.161786 & 1.125098 & 1.523983 \\ 0.649386 & 0.333143 & 2.019611 \end{bmatrix} \\ C &= \begin{bmatrix} 1.040052 & 0.157842 & -0.093433 \\ -0.581603 & 0.837674 & 0.134128 \\ -0.535618 & -0.025389 & 1.049268 \end{bmatrix} \end{aligned}$$

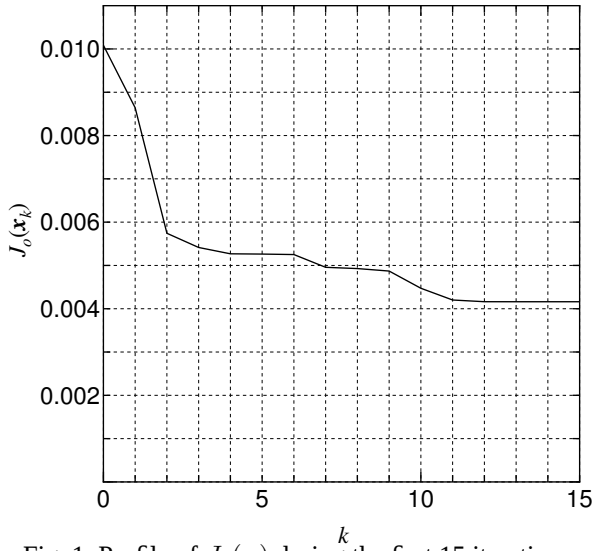


Fig. 1 Profile of $J_o(x)$ during the first 15 iterations.

with which the normalized noise gain was reduced to $J_o(x) = 4.161830 \times 10^{-3}$. The profile of $J_o(x)$ during the first 15 iterations of the algorithm is depicted in Fig. 1. The performance of the iterative algorithm in terms of the normalized noise gain $J_3(C, \hat{T})$ in (36) was compared with that achieved by a separate optimization technique for two implementation settings. The numerical results for the two implementation settings are summarized in Table 1 where the column with "Infinite Precision" shows the value of $J_3(C, \hat{T})$ derived from the optimal $\hat{T}$ and C . The column with "Integer Quantization" means that of $J_3(C, \hat{T})$ where each entry of the optimal C was rounded to an integer and $\hat{T}$ still remains optimal. From the table, it is observed that the iterative optimization technique consistently outperforms the separate optimization technique.

Table 1 Performance comparison of two roundoff noise minimization techniques.

Optimization	Infinite Precision	Integer Quantization
Separate	5.132825×10^{-4}	39.236503×10^{-4}
Iterative	1.926278×10^{-4}	25.238441×10^{-4}

5. CONCLUSION

This paper has investigated the optimization problem of EF and realization to minimize the roundoff noise subject to l_2 -scaling constraints in a system in which full-order state observer feedback is used in place of system state feedback. It has been shown that joint optimization of EF and realization is not needed when utilizing a general-matrix EF loop, because the optimal EF matrix, in closed-form, can be determined in advance. An efficient iterative technique for obtaining the optimal coor-

dinate transformation matrix that minimizes the roundoff noise has been developed by employing a quasi-Newton algorithm. Numerical experiments have demonstrated the validity and effectiveness of the proposed technique and has demonstrated its performance.

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